

PAPER • OPEN ACCESS

The impact of fuelling and W radiation on the performance of high-power, ITER-baseline scenario plasmas in JET-ILW






To cite this article: A R Field *et al* 2021 *Plasma Phys. Control. Fusion* **63** 095013

View the [article online](#) for updates and enhancements.

You may also like

- [Feedback controlled, reactor relevant, high-density, high-confinement scenarios at ASDEX Upgrade](#)
P.T. Lang, T.C. Blanken, M. Dunne et al.
- [Self-consistent simulation of plasma scenarios for ITER using a combination of 1.5D transport codes and free-boundary equilibrium codes](#)
V. Parail, R. Albanese, R. Ambrosino et al.
- [Investigation of key parameters for the development of reliable ITER baseline operation scenarios using CORSICA](#)
S.H. Kim, T.A. Casper and J.A. Snipes

The impact of fuelling and W radiation on the performance of high-power, ITER-baseline scenario plasmas in JET-ILW

A R Field^{1,*} , S Aleiferis², É Belonohy^{1,3}, P Carvalho⁴, I Coffey⁵, D Frigione⁶, L Garzotti¹ , L Horvath¹ , Hyun-Tae Kim^{1,7}, M Lennholm⁸, E Lerche^{1,9}, P Lomas¹, C G Lowry⁸, J Mailloux¹, F Rimini¹, C M Roach¹ , M Sertoli³, Ž Štancar^{2,11}, G Szepesi¹, D van Eester⁹  and JET Contributors¹²

¹ EUROfusion Consortium, JET, Abingdon, Oxon OX14 3DB, United Kingdom

² CCFE, Culham Science Centre, Abingdon, Oxon OX14 3DB, United Kingdom

³ NCSR 'Demokritos' 153 10, Agia Paraskevi Attikis, Athens, Greece

⁴ Max-Planck-Institut für Plasmaphysik, Boltzmannstrasse 2, D-58748 Garching, Germany

⁵ IPFN, Instituto Superior Técnico, Universidade de Lisboa, 1049-001 Lisboa, Portugal

⁶ Department of Pure and Applied Physics, Queens University Belfast, Belfast BT7 1NN, United Kingdom

⁷ Associazione ENEA, Fusion and Nuclear Safety Department, C R Frascati, Via E. Fermi 45, 00044 Frascati (Roma), Italy

⁸ EUROfusion Programme Management Unit, Culham Science Centre, Abingdon OX14 3DB, United Kingdom

⁹ European Commission, B-1049 Brussels, Belgium

¹⁰ LPP-ERM-KMS, EUROfusion Consortium Member–Trilateral Euregio Cluster, TEC Partner, Brussels, Belgium

¹¹ Slovenian Fusion Association (SFA), Joseph Stefan Institute, Jamova 39, SI-1000 Ljubljana, Slovenia

E-mail: anthony.field@ukaea.uk

Received 28 April 2021, revised 14 June 2021

Accepted for publication 16 July 2021

Published 11 August 2021



CrossMark

Abstract

Sustained operation of high-performance, ITER-baseline scenario plasmas at the high levels of input power ($\lesssim 40$ MW) required to achieve ~ 15 MW of D-T fusion power in JET-ILW requires careful optimisation of the fuelling to avoid an unacceptable disruption rate due to excessive radiation, primarily from W impurities, which are sputtered by edge-localised modes (ELMs) from the divertor targets. By using a train of ELM-pacing pellets from a high-frequency pellet injector to promote regular ELMs, which flush W and other impurities from the confined plasma, such high-performance plasmas can be sustained (for ~ 5 s) while maintaining a high normalised confinement factor $H_{98,2} \sim 1$, which would otherwise be degraded by reducing the

¹² See the author list of Joffrin E *et al* 2019 *Nucl. Fusion* **59** 112021.

* Author to whom any correspondence should be addressed.



Original Content from this work may be used under the terms of the [Creative Commons Attribution 4.0 licence](https://creativecommons.org/licenses/by/4.0/). Any further distribution of this work must maintain attribution to the author(s) and the title of the work, journal citation and DOI.

pedestal confinement if a higher rate of D₂ gas fuelling were used instead of the pellets to mitigate the W contamination. The causes underlying the improved performance and energy confinement obtained using this combined, gas and pellet fuelling scheme is investigated here in some detail.

Keywords: JET-ILW, scenario, H-mode, tungsten, fuelling, ITER-baseline, pellets

(Some figures may appear in colour only in the online journal)

1. Introduction

High-performance plasma scenarios are being prepared for the achievement of high levels of fusion power $P_{DT} \lesssim 15$ MW sustained for ~ 5 s in a future D-T campaign on JET-ILW. Two different ELMy H-mode scenarios are under preparation: the ITER-baseline scenario operating at $\beta_N \sim 1.8$ –2 and low edge safety factor $q_{95} \sim 3$ and the hybrid scenario with $\beta_N \sim 2$ –3 and high $q_{95} \sim 4$ [1]. High input powers of $P_{in} \lesssim 40$ MW, primarily from neutral beam injection (NBI) heating are required to achieve such a level of fusion power. Hence, one of the key-performance indicators (KPI) for the current C38 experimental campaign is to achieve a D-D neutron rate $\Gamma_{n,DD} \sim 5 \times 10^{16} \text{ ns}^{-1}$ (equivalent to $P_{DT} \sim 15$ MW) sustained for 5 s in either scenario.

Early experience with high-Z (Mo or W) target materials, e.g. low-density experiments on the PLT tokamak with Mo limiters, showed that core accumulation of only small concentrations ($\sim \mathcal{O}(10^{-4})$) of such impurities could cause radiative collapse of the plasma [2]. It was later realized that tritium retention by co-deposition onto graphite plasma-facing components (PFCs) would pose an unacceptable hazard in ITER or a reactor, so the use of high-Z PFCs was again revisited, with trials of W as a target material in ASDEX-U [3], leading later to successful demonstration of high-density divertor operation of H-mode plasmas with a full metal wall.

At the ~ 40 MW power levels required to demonstrate this KPI in JET-ILW with the all-metal (Be and W) wall, a high fraction of the input power $\mathcal{F}_{Rad} \lesssim 40\%$ is typically radiated, primarily by W impurities in the confined plasma, which are sputtered from the divertor targets by ELMs. Due to the very high emissivity of partially ionized W impurities at electron temperatures in the range 1–10 keV, which is $\times \mathcal{O}(50)$ that of any of the other elements in typical plasma facing materials [4], only tiny concentrations of W $C_W (= n_W/n_e) \sim \mathcal{O}(10^{-4})$ are able to radiate this level of power.

Hence, it is essential to take mitigating measures to avoid excessive W impurity erosion from the targets and to prevent accumulation of the W and other high-Z impurities (Ni, Cu and Fe) into the plasma core, where it can result in hollowing of the electron temperature T_e profile and radiation induced disruption of the plasma due to the triggering of tearing modes [5]. Possible mitigation measures, aimed at reducing the W impurity influx by reducing the temperature at the targets, include: sweeping of the strike-point location; increasing the gas fuelling rate and seeding with a low-Z impurity gas, e.g. Ne or N₂. Ion-cyclotron-resonance heating (ICRH) is

also used to heat the core plasma to mitigate high-Z impurity accumulation [6].

In the baseline scenarios discussed here [1], the strike point location on the outer target is swept radially by $\Delta R \sim 3$ cm at 4 Hz, which is sufficient to prevent excessive local heating of the W coated, graphite tile (T6) and hence avoid melting and vaporisation of the W coating of the carbon-fibre-reinforced graphite (CFC) tiles.

A relatively high level of D₂ gas puffing into the main chamber ($\Gamma_{D2} \sim 2$ – $3 \times 10^{22} \text{ e s}^{-1}$) increases the ELM frequency to typically $f_{ELM} \sim 20$ –50 Hz and hence the rate of W flushing from the confined plasma. Also, the higher particle flux along the scrape-off layer (SOL) increases D⁰ recycling in the divertor, reducing T_i at the target and thereby the inter-ELM sputtered W influx.

A deleterious effect of using a higher D₂ puffing rate is to reduce the pedestal temperature [7] by increasing the conducted power across the pedestal between the ELMs [8, 9], which reduces the pedestal pressure [10] and thereby the overall confinement. Increasing the fuelling rate increases the density at the separatrix $n_{e,sep}$ relative to that at the pedestal top $n_{e,ped}$ [11]. This flattens the n_e gradient across the pedestal, thereby increasing the parameter $\eta_e = L_{n_e}/L_{T_e}$ (where e.g. $L_{n_e} = n_e/n'_e$ and $n'_e = \partial n_e/\partial r$), which provides the drive for turbulent heat transport [12–14]. Also, if the pedestal heat transport is ‘stiff’, i.e. clamped at a threshold η_e required to destabilise turbulent transport, a consequence is that an increased ratio of separatrix to pedestal density $n_{e,sep}/n_{e,ped}$ would also result in a lower temperature $T_{e,ped}$ at the pedestal top [8].

ICRH also has to be used in high-power H-mode JET-ILW discharges, both to avoid core impurity accumulation, particularly during the plasma termination, and to promote an early L/H transition [6, 15]. By using distributed main-chamber fuelling to optimize antenna-plasma coupling, an RF power $P_{RF} \sim 4$ –6 MW can be routinely coupled into the plasma, minimizing the RF-induced plasma-wall interactions due to sheath-rectification effects.

Central ICRH power deposition and low concentrations of the H⁺ minority ions give the best results for core electron heating, achieving absorption efficiencies up to $\sim 90\%$. In these conditions, peaked temperature profiles, together with relatively flat density profiles, allow efficient high-Z impurity screening to be achieved with $P_{RF} \gtrsim 4$ MW.

In spite of these mitigation measures, excessive W radiation can still hamper the achievement of steady, ELMy H-mode operation at high power. Unstable plasma conditions caused by runaway radiation ‘events’, result in an unacceptably high

rate of disruptions, which are particularly dangerous to the device at the high plasma currents ($I_p \sim 3\text{--}4.5$ MA) typical of the ITER-baseline scenario pulses.

The role of W radiation cooling in the termination of ITER-baseline pulses in JET-ILW has been investigated statistically [5]. Depending on whether the W radiates from the plasma core or periphery, the resulting broadening or shrinking of the current profile, increases the probability of destabilising 2/1 tearing modes, which can induce disruptions. This analysis is used to develop disruption alerts based on T_e -profile shape parameters. Here, we investigate the underlying mechanism of these processes in terms of the behaviour of the W impurities.

The W content of the plasma, and hence the level of radiation, is governed by a balance between the ingress of W impurities from the SOL by inward neo-classical convection across the pedestal and their removal *aka* ‘flushing’ from the plasma by ELMs. Too high a fraction of W radiation can dominate the plasma power balance, reducing the ELM frequency, allowing a further increase of the W content. This ‘vicious circle’ can either trigger an H/L-transition and subsequent W accumulation or cause radiative cooling and MHD-induced collapse from the plasma edge.

Fortuitously, the relatively high plasma current $I_p \sim 3\text{--}4.5$ MA of baseline-scenario pulses compared to that of hybrid pulses $\sim 2.2\text{--}2.3$ MA results in a high pedestal density $n_{e,ped}$ and, consequently, a rather flat core density profile, which favours outward neo-classical impurity convection *aka* ‘screening’, localising the impurities to the peripheral ‘mantle’ region of the plasma, which corresponds approximately to the outer third of the plasma radius, inside the pedestal top (see figure 2 and associated discussion for the definition of these regions). This screening is not so effective in hybrid scenario pulses, which typically have more peaked density profile.

In hybrid pulses, accumulation of high-Z impurities, triggered by low- n neo-classical tearing modes (NTMs) [16], which are destabilised by the higher poloidal- β , $\beta_p \sim 1.0$ of these plasmas compared to that of baseline pulses ($\beta_p \sim 0.6$), has hampered sustained, high-performance operation. By optimising the gas fuelling during the initial current ramp phase, it has recently been demonstrated that, with sufficient heating power, it is possible to achieve a hot, low collisionality pedestal, resulting in sufficiently strong T'_i at the pedestal to screen out the W from the confined plasma, thereby effectively mitigating this problem [17].

Such unstable, radiative conditions can be avoided by triggering regular ELMs by the injection of a train of small, cryogenic D₂ ‘ELM-pacing’ pellets, thereby maintaining the rate of W flushing from the confined plasma. For this purpose, a high-frequency pellet injector is available on JET-ILW for injection of both ELM-pacing and fuelling pellets [18, 19]. The small ($\sim 2\phi$ mm) pacing pellets can be injected at frequencies $f_{Pel} \sim 10\text{--}45$ Hz from a flight line located at the upper high-field side (HFS) of the main vessel.

Partially replacing some of the gas fuelling by injection of such ELM-pacing pellets, typically resulting in a lower total fuelling rate, is found both to extend the duration of the ELMy H-mode phase and to enhance the overall confinement compared to that achieved with gas fuelling alone [1]. Here, we

investigate the underlying causes of both the improved confinement and extended duration of the high-performance phase of high-power, baseline-scenario pulses obtained using a combination of D₂ gas fuelling and ELM-pacing pellets.

In order to illustrate the effect of the level of gas fuelling on the performance of high-power, ITER-baseline scenario, H-mode pulses in JET-ILW, in section 2, we compare the evolution of three similar 3.5 MA pulses with injected heating power $P_{in} \sim 29\text{--}33$ MW, two with low and high rates of gas fuelling ($\Gamma_{D2} \sim 1.5$ and $2.3 \times 10^{22} \text{ es}^{-1}$) and a third with ELM pacing pellets (at a requested repetition frequency of $f_{Pel} \sim 45$ Hz) with a total fuelling rate from gas puffing and pellets matching that of the pulse with the higher fuelling rate.

In section 2.1, kinetic profiles are shown for two of the pulses discussed in section 2 to compare the core and pedestal confinement achieved with either gas-fuelling alone or pellet + gas fuelling. Detailed results on the ion and electron power balances and the momentum balance, which are obtained from an interpretive transport analysis using TRANSP, are presented in section 2.2 and the effect of the fuelling on the core heat and momentum transport is investigated in section 2.3.

In section 2.4, the effect of the ELM flushing on the W content and the evolution of the total radiation is investigated. Firstly, in section 2.5, the method used to quantify the W flushing by the ELMs, based on an analysis of fast bolometric measurements of the radiated power, is explained. Results from application of this analysis to a high-power, gas-fuelled 3 MA pulse #92 432, which also exhibits a core W accumulation ‘event’, are presented in section 2.6. In section 2.7 results of the ELM-flushing analysis from the pulses discussed in section 2 are then compared.

By classifying the ELMs as either ‘pellet-triggered’ or spontaneous, ‘natural’ events, we can investigate the influence of the ELM type on their efficiency at flushing the W impurities. In section 2.8, a statistical analysis of the ELM flushing and inter-ELM ingress of W, is presented, classifying the data by ELM type.

As the ELM-sputtered, ‘intra-ELM’ W impurity source dominates that during the inter-ELM periods, in section 2.9 we compare relative intra-ELM Be and W impurity fluences $\Phi_{Be,W}$, i.e. the influxes integrated over the ELM duration, for the different ELM types. These are evaluated from visible Be II and WI line intensities from a multi-channel spectrometer viewing the divertor targets.

In order to determine whether any of the improvements in plasma performance caused by modification of the W behaviour is induced by the pellets, the effect of the pacing pellets on the inter-ELM evolution of the kinetic profiles (and associated gradient parameters) in the pedestal and mantle regions is investigated in section 2.10.

In the discussion section 3, a mechanism is proposed in section 3.1 for the interaction of fuelling, ELMs and W impurities in high-power, ITER-baseline pulses, which is then applied to understanding the radiation event in pulse #92 432 in section 3.2. The possible influence of fuelling on the retention of sputtered impurities in the divertor is discussed in section 3.3.

Table 1. Parameters of analysed 3.5 MA/3.3 T ITER-baseline scenario pulses, showing: total heating power P_{in} ; fuelling rates Γ_{D2} from gas puffing, pacing pellets and total; the requested ELM-pacing pellet frequency f_{Pel} ; peak plasma stored energy $W_{pl,max}$; peak D-D neutron rate $\Gamma_{n,DD}$; duration of 80% peak-performance, ELMy H-mode phase Δt_{HP} ; and the concentrations C_{min} of H and ^3He minority ions for the ICRH.

Pulse #	P_{in} (MW)	$\Gamma_{D2} \times 10^{22} \text{ (s}^{-1}\text{)}$			f_{Pel} (Hz)	$W_{th,max}$ (MJ)	$\Gamma_{n,DD}$ $10^{16} \text{ (s}^{-1}\text{)}$	Δt_{HP} (s)	C_{min}	
		Gas	Pellet	Total					H (%)	^3He (%)
94 915	28	1.5	—	1.5	—	8.8	2.2	~ 1	~ 1.5	—
94 980	29	2.3	—	2.3	—	7.5	1.2	~ 3	~ 1	~ 2.5
96 713	33	1.0	1.3	2.3	45–35	10.5	3.5	~ 3	~ 3	—

Finally in section 4, we present the main conclusions of this study and an outlook to future work.

2. Comparison of high-power, 3.5 MA pulses with different fuelling sources

To illustrate the importance of optimising the particle fuelling in achieving maximal energy confinement (and hence fusion yield) and pulse duration at high-performance, in this section, the evolution of three, 3.5 MA ITER-baseline (BL) scenario pulses with 29–33 MW of additional heating power are compared. Two of these, #94 915 and #94 980 have low and high rates of D_2 gas fuelling during the sustained H-mode phase of $\Gamma_{D2} \sim 1.5$ and $2.3 \times 10^{22} \text{ es}^{-1}$ respectively from gas-inlet modules at octants #1, 6 and 8) in the main chamber. The other pulse #96 713 has both D_2 gas fuelling at a low rate of $\sim 1.0 \times 10^{22} \text{ es}^{-1}$ and D_2 ELM-pacing pellets. The key parameters of these three pulses are given in table 1 and a comparison of their evolution is shown in figure 1.

The D_2 pellets used for triggering, *aka* ‘pacing’ ELMs on JET-ILW have dimensions $\phi 2$ mm and length ~ 2 mm with an average particle content $\Phi_{D2,pel} \sim 3 \pm 0.2 \times 10^{20} \text{ e/pellet}$, measured by the last microwave cavity along the flight tube. At the requested pellet rate of $f_{Pel} \sim 45$ Hz for pulse #96 713, this results in a time-averaged fuelling rate into the vessel of $\Gamma_{D2,pel} \sim 1.3 \pm 0.2 \times 10^{22} \text{ es}^{-1}$. As shown in figure 1(b), the resulting total, time-averaged fuelling rate from the gas and pellets $\Gamma_{D2} = \Gamma_{D2,gas} + \Gamma_{D2,pel} \sim 2.2 \times 10^{22} \text{ es}^{-1}$ almost matches that in pulse #94 980 with the higher rate of gas fuelling alone.

Although the thermal stored energy W_{th} is somewhat higher ($\sim 15\%$) in pulse #94 915 than in pulse #94 980 with the higher fuelling rate, i.e. ~ 8.8 MJ cf ~ 7.5 MJ, as shown in figure 1(e) pulse #94 915 is non-stationary, exhibiting complex ELM behaviour, with some large, type-I ELMs, each followed by a period of small ELMs and then a long ELM-free phase of duration ~ 0.2 s. During the final ELM-free, H^* -phase, the radiated power fraction \mathcal{F}_{Rad} (see figure 1(a)) increases to $\gtrsim 40\%$ of the input power, at which point this triggers a controlled termination of the pulse, which commences with a strong increase of the gas puffing rate (not shown).

Stronger gas puffing into the main chamber is required to achieve steady operation, e.g. as in pulse #94 980, resulting in more frequent, smaller amplitude, type-I ELMs, some of which are followed rapid bursts of small, type-III ELMs and subsequent, shorter H^* -phases, as shown in figure 1(f).

A relative measure of the time-averaged ($\tau_{sm} = 0.25$ s) ELM-sputtered Be II influx $\langle \Gamma_{Be} \rangle \propto \langle I_{BeII} \rangle$ shown in the figure (cyan), indicates that the impurity source is, on-average, probably not very different to that in the non-stationary pulse #94 915. However, the more frequent ELMs manage to expel sufficient of the highly radiative W impurities to maintain $\mathcal{F}_{Rad} \lesssim 30\%$ (see figure 1(a)).

The achievement of sustained, ELMy H-mode operation at high-power with the stronger gas puffing does, however, come at the cost of reduced pedestal temperature and, consequently, lower overall energy confinement (see [8] and references therein.) The effect of the different fuelling on the pedestal parameters in these pulses is quantified in section 2.10 below. In terms of the normalised confinement, as shown in figure 1(c), the H-mode confinement enhancement factor $H_{98,y2}^{12}$ is reduced by the stronger gas puffing to ~ 0.8 cf ~ 1.0 in pulse #94 915, while the input power in these two pulses is similar $P_{in} \sim 29$ MW.

Note that, although the rates and method of fuelling are different, the achieved, line-average density $\bar{n}_e \lesssim 0.8 \times 10^{20} \text{ m}^{-3}$ (corresponding to a Greenwald density fraction $f_{GW} = \bar{n}_e/n_{e,GW} \lesssim 0.7^{13}$) is similar in these three pulses. The line-averaged, effective ion charge $Z_{eff} \sim 1.6$, inferred from a horizontal mid-plane, visible bremsstrahlung measurement, is also similar for the three pulses.

As shown in figure 1(d), the $\sim 50\%$ reduction in the D-D neutron rate $\Gamma_{n,DD}$ caused by the increased gas puffing rate in pulse #94 980 is more severe than the reduction in thermal energy, the former being $\Gamma_{n,DD} \lesssim 1.0 \times 10^{16} \text{ ns}^{-1}$ c.f. $\lesssim 2.0 \times 10^{16} \text{ ns}^{-1}$ in pulse #94 915. This is a consequence of the lower peak ion temperature $T_{i,0} \sim 6$ keV in pulse #94 980 compared to ~ 8 keV in pulse #94 915 and the fact that the Maxwell-averaged rate coefficient $\langle \sigma_{DD} \rangle$ increases strongly with temperature (approximately $\propto T_i^2$) [20].

The injection of ELM-pacing pellets to trigger ELMs in conditions which would otherwise result in long H^* -phases (and potentially a high disruptivity) offers a means of extending the duration of the high-performance, ELMy H-mode phase, whilst maintaining the high pedestal temperature and

¹² The H-mode confinement enhancement factor $H_{98,y2}$ is defined as the ratio of the thermal energy confinement time $\tau_{E,th}$ to the energy confinement time $\tau_{E,98y2}$ from the ITER $H_{98,y2}$ energy confinement scaling [21], i.e. $H_{98,y2} = \tau_{E,th}/\tau_{E,98y2}$.

¹³ The Greenwald density is defined as $n_{e,GW} = I_p/(\pi a^2)$, where I_p is the plasma current in MA and a is the geometrical minor radius in m.

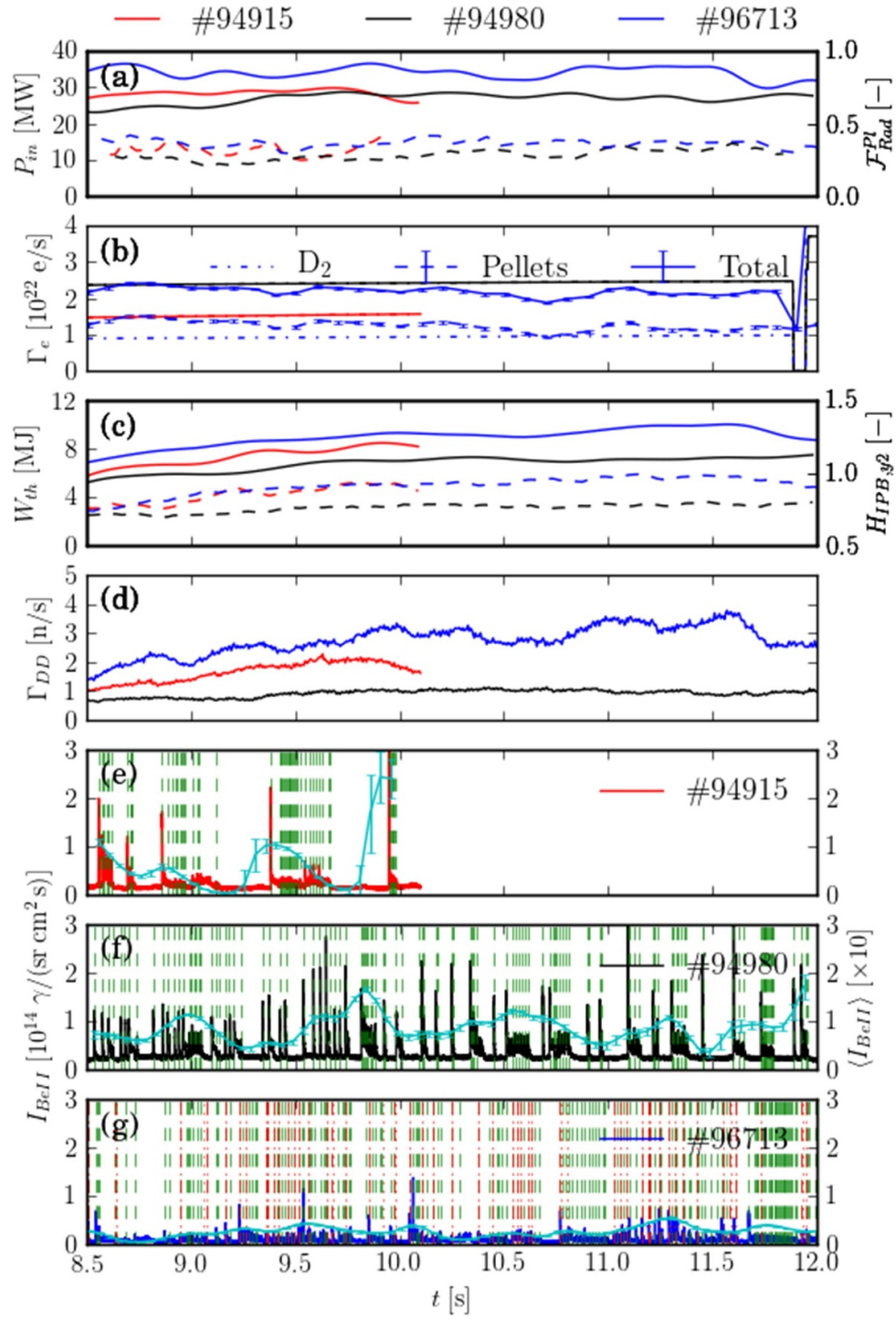


Figure 1. Comparison of evolution of 3.5 MA/3.3 T ITER-baseline scenario pulses with different fuelling sources #94 915 (red), #94 980 (black) and #96 713 (blue) with the key parameters given in table 1 showing: (a) total injected heating power P_{in} and radiated power fraction $\mathcal{F}_{Rad} = P_{Rad}/P_{abs}$; (b) fuelling rates Γ_{D2} (e s^{-1}) from D_2 gas $\Gamma_{D2,gas}$ (dot-dashed), pacing pellets $\Gamma_{D2,pel}$ (smoothed, $\tau_{sm} = 0.25$ s) (dashed) and total fuelling rate $\Gamma_{D2} = \Gamma_{D2,gas} + \Gamma_{D2,pel}$ (solid); (c) total MHD stored energy W_{th} (solid) and H-mode confinement enhancement factor $H_{98,y2}$ (dashed); (d) total D-D neutron rate $\Gamma_{n,DD}$; (e)–(g) the ELM behaviour from a visible Be II line viewing the outer divertor target, where the smoothed ($\tau_{sm} = 0.25$ s), intra-ELM integrated signal $\langle I_{BeII} \rangle$ is also shown (cyan, $\times 10$) and the ELM peaks are marked by the vertical lines (natural ELMs (dashed/green) and pellet triggered ELMs (red/dot-dashed)).

Table 2. Average pedestal parameters over the high-performance, ELMy H-mode phase of the same three pulses (#94 915, #94 980 and #96 713) for which key parameters are stated in table 1 over the period $t_0 \rightarrow t_1$. Further details of how these parameters are determined are given in section 2.10. Note that the value of $\Omega_{\phi,ped}$ is that of Ω_{ϕ} at the top of the n_e pedestal, while the density ratio $n_{e,sep}/n_{e,ped}$ is determined by assuming a fixed value of $T_e \sim 100$ eV at the separatrix.

Pulse #	$t_0 \rightarrow t_1$ (s)	$\langle T_{e,ped} \rangle$ (keV)	$\langle n_{e,ped} \rangle$ ($\times 10^{20} m^{-3}$)	$\langle T_{i,ped} \rangle$ (keV)	$\langle \Omega_{\phi,ped} \rangle$ ($\times 10^5$ r s $^{-1}$)	$\frac{\langle n_{e,sep} \rangle}{\langle n_{e,ped} \rangle}$ (—)
94 915	8.5–10.0	0.78 ± 0.02	0.52 ± 0.02	1.17 ± 0.03	23.1 ± 0.8	0.18 ± 0.03
94 980	10.0–12.0	0.81 ± 0.01	0.59 ± 0.01	1.07 ± 0.02	21.9 ± 0.5	0.23 ± 0.01
96 713	10.0–12.0	0.76 ± 0.03	0.48 ± 0.01	1.00 ± 0.02	24.3 ± 0.6	0.20 ± 0.01

overall confinement that is achieved at lower gas fuelling rates. In the pulse #96 713 the gas fuelling rate of $\Gamma_{D2,gas} \sim 1.0 \times 10^{22} \text{ e s}^{-1}$ is lower than that in pulse #94 915 but the total fuelling rate, including that from the 45 Hz pellets is close to that from the gas puffing alone in #94 980.

As shown in figure 1(g), this combined fuelling scheme results in higher frequency, lower amplitude ELMs, even than those in the pulse #94 980 with the higher fuelling rate. Although most but not all pellets trigger ELMs, the overall ELM frequency does not lock to the pellet frequency. Instead, there are typically bursts of small amplitude, high-frequency ELMs that follow the pellet triggered ELMs, resulting in a higher average ELM frequency than that of the pellets.

As a result of the small ELM amplitude, the time-averaged, relative ELM-sputtered Be II influx $\langle \Phi_{Be} \rangle$ is lower than in either of the other two pulses with the gas fuelling alone. In spite of this, the radiated power fraction $\mathcal{F}_{Rad} \lesssim 40\%$ is higher than in the high-gas pulse #94 980, lying just below that required to trigger an early pulse termination by the safety interlock. Note that the duration of the pulse with gas and pellets #96 713 is not limited by a high radiation fraction or W accumulation but intentionally by the control system, which was programmed to commence pulse termination by strongly increasing the gas puffing rate at 52 s.

The pulse #96 713, with gas and pellet fuelling, has a higher input power of 33 MW, i.e. $\sim \times 1.15$ more than the ~ 29 MW in the pulses with gas puffing alone. The resulting stored energy $W_{th} \lesssim 10.5$ MJ is relatively higher than in the two gas-fuelled pulses with low and high puffing rates, in which $W_{th} \sim 8.8$ MJ and ~ 7.5 MJ respectively. The confinement enhancement factor $H_{98,y2}$, which offers a means of comparing the quality of confinement taking into account the difference in heating power, is restored to the same level in the pulse #96 713 with gas and pellets to that in the low-gas pulse #94 915, i.e. $H_{98,y2} \lesssim 1.0$.

Remarkably, at the same stage of the pulse, the D-D neutron rate is considerably higher ($\sim \times 1.5$) in pulse #96 713 with the pellets and gas than in the low-gas pulse #94 980, i.e. by a much larger factor than that of the extra heating power. In the next section section 2.1, we show that this can be attributed to a higher axial ion temperature $T_{i,0}$, which may result from increased rotational shear across the core plasma due to an overall higher toroidal rotation rate Ω_{ϕ} . The enhanced rotation in pulse #96 713 may in part arise from the $\sim \times 1.1$ higher

rotation at the pedestal top $\Omega_{\phi,ped}$ (see table 2 and figure 11(f) below).

The higher core T_i increases the D-D neutron rate coefficients $\langle \sigma_{DD} \rangle$ for both thermal and beam-target D-D fusion reactions, the latter causing the beam-target neutron rate to increase more strongly than linearly with the NBI heating power. Typically, in such high-power, 3.5 MA baseline-scenario pulses in JET-ILW, beam-target reactions contribute $\sim 30\%$ – 40% of the total D-D neutron rate.

It is conjectured that the increase in Ω_{ϕ} at the plasma periphery may be due to reduced charge-exchange (CX) friction with neutral D^0 atoms due to the lower rate of main-chamber gas puffing used in #96 713. As the pellets provide $\sim 50\%$ of the fuelling and are injected at the HFS, while the main-chamber gas puffing at the low-field side (LFS) is reduced, a lower D^0 density at the LFS would result in less frictional drag on the plasma [22].

2.1. Comparison of energy confinement in pulses #94 980 and #96 713

A beneficial effect of operating at a reduced gas fuelling rate with the ELM pacing pellets is an enhancement of the core energy confinement, which is associated with increased toroidal rotation and reduced ion temperature gradient stiffness [23]. A comparison of kinetic profiles averaged over a 2 s period of the ELMy H-mode phase of the 3.5 MA ITER-baseline pulses #94 980 with only gas fuelling and pulse #96 713 with pellets + gas fuelling is shown in figure 2. As stated previously in section 2, these pulses have similar total fuelling rates of $\Gamma_{D2} \sim 2.3 \times 10^{22} \text{ e s}^{-1}$, however, the pulse #96 713 has only $\sim 43\%$ of the gas fuelling rate $\Gamma_{D2,gas}$ of #94 980.

These profiles are from an interpretive transport analysis using the TRANSP code [24] based on input kinetic profiles which are mapped onto the radial coordinate $\rho_{tor} = \sqrt{\Phi_N}$, where Φ_N is the normalised toroidal flux using a pressure-constrained, magnetic equilibrium obtained from the EFIT++ equilibrium reconstruction code [25, 26]. More details of the TRANSP run, including the origin of the input data and the assumptions made are given in section 2.2.

It can be seen from figure 2(a), that across the core plasma, both the ion temperature T_i and the toroidal rotation rate Ω_{ϕ} are higher in the pellet + gas-fuelled pulse #96 713 than in the

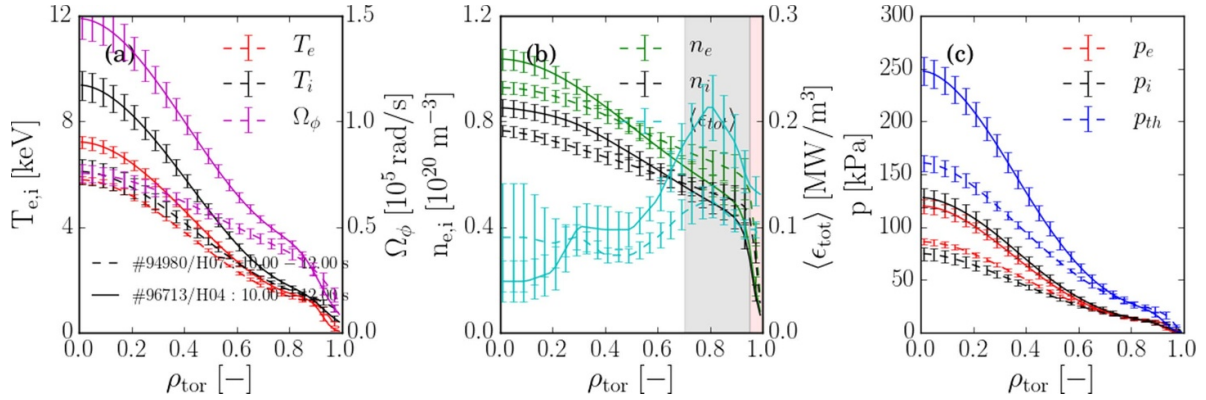


Figure 2. Comparison of fitted, time-averaged kinetic profiles for two of the three pulses shown in figure 1 #94 980 (high gas fuelling rate) and #96 713 (pellet and gas fuelling, with total rate matched to that for #94 980) showing radial profiles vs ρ_{tor} of: (a) ion and electron temperatures $T_{i,e}$ and toroidal rotation Ω_ϕ rates; (b) ion and electron densities $n_{i,e}$ and flux-surface averaged total emissivity $\langle\epsilon_{tot}\rangle$; (c) ion, electron $p_{i,e}$ and total thermal p_{th} pressures. The radial coordinate $\rho_{tor} = \sqrt{\Phi_N}$, where Φ_N is the normalised toroidal magnetic flux. The radial extents of the mantle and pedestal regions are indicated by the shaded bars in (b).

Table 3. Thermal stored energies (total and of either ions or electrons) of the whole plasma and that due to the pressures at the pedestal top, averaged over the period 50.0 \rightarrow 52.0 s during the high-performance, ELMy H-mode phase of the two pulses (#94 980 and #96 713) for which key parameters are stated in table 1. Also stated are the time-averaged ratios of total ion to electron heating power $\langle P_i/P_e \rangle$ and thermal energies of the ions and electrons $\langle W_i \rangle/\langle W_e \rangle$.

Pulse #	$\langle W_{th} \rangle$ (MJ)	$\langle W_e \rangle$ (MJ)	$\langle W_i \rangle$ (MJ)	$\langle W_{th,ped} \rangle$ (MJ)	$\langle W_{e,ped} \rangle$ (MJ)	$\langle W_{i,ped} \rangle$ (MJ)	$\langle P_i/P_e \rangle$ (—)	$\frac{\langle W_i \rangle}{\langle W_e \rangle}$ (—)
94 980	6.53 ± 0.02	3.18 ± 0.01	3.35 ± 0.01	2.00 ± 0.04	0.88 ± 0.02	1.12 ± 0.03	1.18 ± 0.06	1.05 ± 0.01
96 713	8.54 ± 0.05	3.71 ± 0.02	4.84 ± 0.03	1.52 ± 0.03	0.64 ± 0.02	0.88 ± 0.02	1.33 ± 0.07	1.31 ± 0.01

gas fuelled pulse #94 980, on-axis by factors of ~ 1.5 and ~ 2 respectively. However, at the pedestal top, these parameters are approximately equal. It should be noted that the additional heating power P_{in} is $\sim \times 1.13$ higher in #96 713 than in pulse #94 980.

Average values of pedestal parameters over the high-performance, ELMy H-mode phase for the same 3.5 MA pulses as in table 1 are stated in table 2. Note that, in spite of the $\sim \times 2$ higher fuelling rate in pulse #94 980 as in pulse #96 713, the pedestal temperatures for the two pulses are quite similar. However, there are significant differences in the edge rotation and density, with lower $\langle n_{e,ped} \rangle$ by $\sim \times 0.8$ and lower relative separatrix density $\langle n_{e,sep} \rangle/\langle n_{e,ped} \rangle$ by $\sim \times 0.9$ but higher $\langle \Omega_{\phi,ped} \rangle$ by $\sim \times 1.1$ in #96 713 with the pellet + gas fuelling compared to those in #94 980.

Density profiles of the electrons and D^+ ions are shown in figure 2(b). Although $n_{e,ped}$ is $\sim \times 1.1$ higher in the gas-fuelled pulse #94 980 than in the pellet + gas fuelled pulse #96 713, the line-averaged density \bar{n}_e is the same in both pulses, so the density profile is somewhat more peaked in the pellet + gas fuelled pulse #96 713, with $\bar{n}_e/n_{e,ped} \sim 1.67$ compared to ~ 1.35 in #94 980. The effect of the lower pedestal density with the pellet + gas fuelling on the power and momentum deposition from the neutral-beam-injection (NBI) heating is discussed in detail in section 2.2. As a lower $n_{e,ped}$ increases the beam penetration, this will increase the beam particle source in the core, thereby enhancing the density peaking.

Also shown in figure 2(b) are profiles of the flux-surface averaged total emissivity $\langle\epsilon_{tot}\rangle$ from tomographic reconstructions [27] of multi-chord, bolometric measurements of the total radiation [28]. In the peripheral, ‘mantle’ region (defined here as $0.7 \leq \rho_N \leq \rho_{N,ped} \sim 0.96$), we see that $\langle\epsilon_{tot}\rangle$ is $\lesssim \times 1.8$ higher in the pellet + gas fuelled pulse #96 713 than in the gas-only fuelled pulse #94 980, which is consistent with the higher concentration of W in the mantle (see figure 11(a)), which is the dominant radiator in such high-power H-mode pulses in JET-ILW. The effect of this strong mantle radiation on the ion and electron power balances is also discussed in section 2.2.1 (see also section 4 of [8]).

Finally, we see from figure 2(c), that on-axis, the total thermal pressure p_{th} is $\sim \times 1.5$ higher in pulse #96 713 than in pulse #94 980, primarily due to the higher ion temperature $T_{i,0}$, which is $\sim \times 1.5$ higher in #96 713, while $T_{e,0}$ is only $\sim \times 1.23$ higher than in pulse #94 980. The average volume-integrated, total stored energies $\langle W_{th} \rangle$ and those of the ions and electrons $\langle W_e \rangle$ and $\langle W_i \rangle$, obtained from the TRANSP runs for these pulses are stated in table 3, together with the corresponding, averaged pedestal stored energies.

From these stored energies in table 3, we see that on-average, the pedestal energy $\langle W_{th,ped} \rangle$ is $\sim \times 1.3$ higher in the gas fuelled pulse #94 980 than in the pellet + gas fuelled pulse #96 713, primarily due to the higher $n_{e,ped}$ in the former. However, the total stored energy $\langle W_{th} \rangle$ is $\sim \times 1.3$ higher in pulse #96 713, which has $\sim \times 1.13$ higher input power than pulse #94 980. Comparing the ratios of the components of the total

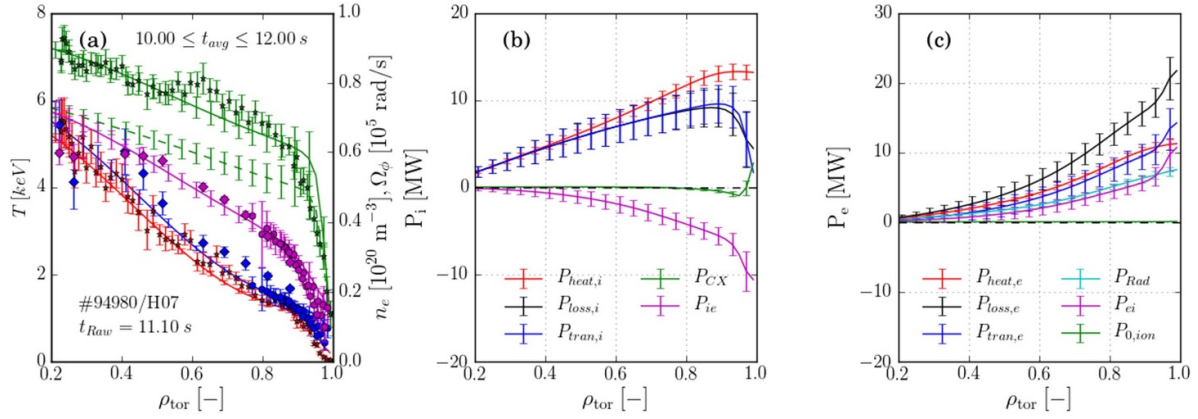


Figure 3. Results of interpretive, power balance analysis using TRANSP of pulse #94980 showing: (a) fitted kinetic profiles T_e (red), n_e (green, solid) and n_i (green, dashed) from HRTS, T_i (blue) and Ω_ϕ (magenta) from the core and edge CXRS systems; radially integrated powers of components of the power balances of the ions (b) and the electrons (c), where the profiles are averaged over the time period $10.0 \leq t \leq 12.0$ s and the error bars represent the standard deviations of the data σ_{data} . A ‘snapshot’ of the raw measurement data is shown at $t_{Raw} = 11.1$ s.

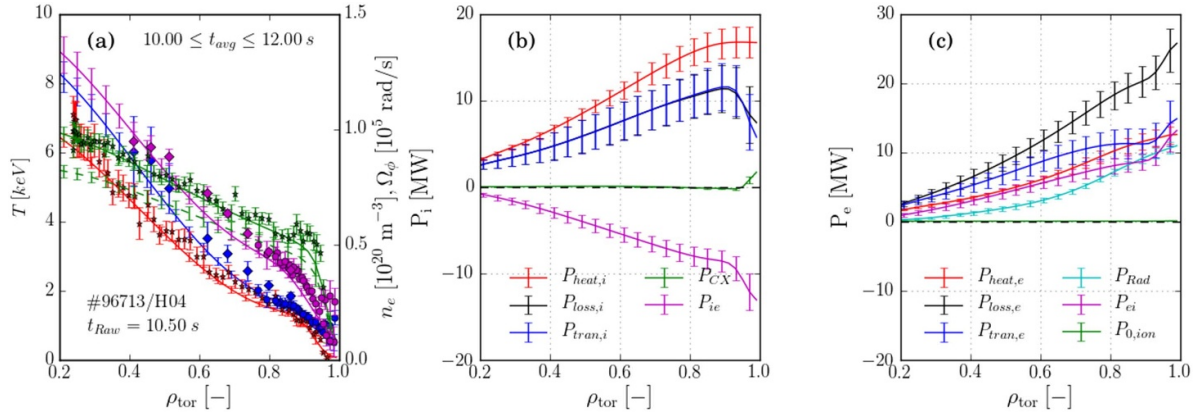


Figure 4. Results of interpretive, power balance analysis using TRANSP of pulse #96713, where the profiles are averaged over the period $10.0 \leq t \leq 12.0$ s and a snapshot of the raw data is shown at $t_{Raw} = 10.5$ s. The definition of the quantities plotted are the same as in figure 3.

thermal energy stored in the ions to that in the electrons, we see that $\langle W_i \rangle / \langle W_e \rangle \sim 1.3$ is higher in pulse #96713 compared to ~ 1.05 in #94980.

This relative increase in ion energy confinement cannot be explained solely by an increase in the average ratio of ion to electron heating $\langle P_i / P_e \rangle$, which is higher in pulse #96713 compared to that in pulse #94980 by a factor ~ 1.12 . Hence, there is also a relative improvement of the ion energy confinement with the pellet + gas fuelling compared to that with gas fuelling alone. The reason for this is discussed in more detail in section 2.3, in which the effect of the changes to the fuelling between pulses #94980 and #96713 on the ion and electron heat transport and the transport of toroidal angular momentum L_ϕ across the core plasma is investigated.

2.2. Power and momentum balance analysis of #94980 and #96713

In this section, results on the power balances of the ions and electrons and the balance of toroidal angular momentum

for the two 3.5 MA pulses: #94980 with the high rate of gas fuelling alone and #96713 with a similar total fuelling rate from gas and ELM pacing pellets, are presented and compared.

The primary input data for the transport analysis are the kinetic profiles (T_e , n_e , T_i and Ω_ϕ), which are obtained by fitting the raw data from the high-resolution Thomson scattering system (HRTS) [29] and the core and edge CXRS systems [30, 31]. The fits use an $\text{mtanh}()$ function to represent the profiles over the pedestal region ($\rho_{N,ped} \sim 0.96 \leq \rho_N \leq 1$) [32] and a third-order polynomial for the core region. Examples of the raw profiles at 11 s are shown in figures 3(a) and 4(a). As the T_i and Ω_ϕ data from the edge CXRS system on JET-ILW is considered more reliable than that from the core system, the outer two points of the core CXRS (not shown) are excluded from the fit.

Pressure constrained EFIT++ equilibrium reconstructions [26] are used to map the measurement data from major radius to the normalised flux coordinate, i.e. $\rho_{tor}(R_m)$. Using these equilibria for the profile mapping, meaningful results can be

Table 4. Time-averaged quantities over 10–12 s from the integrated analysis of impurity radiation described in [34] for the two pulses for which interpretive TRANSP analysis has been performed here, stating volume-averages $\langle \dots \rangle$ of: total Z_{eff} and Be, Ni and W impurity concentrations C_Z , with their incremental contributions ΔZ_{eff} to Z_{eff} and their fractional contributions $\mathcal{F}_{\text{Rad},Z}$ to the total radiated power. The H and ^3He minority ion concentrations C_{min} assumed for the TORIC calculations of the ICRH power deposition are also stated.

Pulse #	$\langle Z_{\text{eff}} \rangle$ —	$\langle C_Z \rangle$ (%)			$\langle \Delta Z_{\text{eff}} \rangle$			$\mathcal{F}_{\text{Rad},Z}$ (%)			C_{min} (%)	
		Be	Ni	W	Be	Ni	W	Be	Ni	W	H	^3He
94 980	1.6 ± 0.03	3.8	0.02	0.005	0.61	0.11	0.05	3.6	17.3	75.5	1	2.5
96 713	1.6 ± 0.03	2.1	0.04	0.01	0.35	0.23	0.12	1.52	12.9	82.5	3	—

obtained in the pedestal region with no additional constraint required to ensure a reasonable value for $T_{e,\text{sep}}$, which is typically ~ 100 eV (see [33]).

For these interpretive transport calculations, time-dependent, radial profiles of flux-surface averaged densities of Be, Ni and W impurities are input to TRANSP, which are obtained from an integrated analysis described in [34], as for similar analysis presented in a previous study [8]. This analysis self-consistently fits bolometric measurements of the total emissivity, multi-channel soft x-ray measurements and a horizontal, visible bremsstrahlung measurement of the line-average Z_{eff} , taking account of the poloidal redistribution of the impurity ions over the flux surfaces by centrifugal forces due to the toroidal rotation.

These calculations, which assume a radially constant concentration of Be impurities, yield the volume averaged quantities for the principle Be, Ni and W impurities, summarised in table 4.

For both pulses the volume-averaged $\langle Z_{\text{eff}} \rangle \sim 1.6$. Pulse #94 980 has twice the concentration of Be ($C_{\text{Be}} \sim 4\%$) than pulse #96 713 ($\sim 2\%$). Conversely, the volume-averaged concentrations of the heavy impurities Ni and W, which are $\mathcal{O}(10^{-4})$ are twice as high in pulse #96 713 than in pulse #94 980 and in both pulses the concentration of Ni is ~ 4 that of W. In spite of this, the W radiates $\gtrsim 75\%$ and the Ni $\lesssim 20\%$ of the total radiated power in both pulses. Although the Be radiates only a few % of the power, this species makes the largest contribution to Z_{eff} .

Power deposition profiles from the NBI and ICRH heating systems are calculated using the codes NUBEAM [35] and TORIC [36]. The ICRH heats the bulk plasma by means of the cyclotron resonance of the RF waves with a minority ion species. In pulse #96 713 there is a single H minority at a concentration of $\sim 3\%$, while for pulse #94 980 there are both H and ^3He minority ions at average concentrations of $\sim 1\%$ and $\sim 2.5\%$ respectively. The presence of the heavier ^3He minority species is to increase fraction of ICRH power heating to the D^+ ions.

The neutral D^0 influx at the plasma boundary, which determines the edge ionisation source, is determined from a horizontal, mid-plane D_α intensity measurement by assuming a ratio of ionisations/photon $S/XB = 10$. Note that the TRANSP runs, from which the results are reported here, do not account for the particle source from the ablation of the D^0 pacing pellets, which are injected at the upper-HFS of the main vessel.

In the following discussion, we refer to volume integrated forms of the power and momentum balances, e.g. for the power balance, the corresponding power P_X is calculated from the power density Q_X for quantity X as $P_X(\rho'_N) = \int_0^{\rho'_{\text{tor}}} Q_X(dV/d\rho_{\text{tor}}) d\rho_{\text{tor}}$ to yield the associated power deposited within or leaving the ρ'_{tor} flux surface.

We can define two further powers for the ions: the loss power due to ion heat transport $P_{\text{tran},i} = P_{\text{cond},i} + P_{\text{conv},i}$, where $P_{\text{cond},i}$ and $P_{\text{conv},i}$ are the conducted and convected powers, and the total loss power from the ions $P_{\text{loss},i} = P_{\text{tran},i} + P_{\text{cx}}$, where P_{cx} is the CX loss power. Similarly for the electrons: the power due to electron heat transport $P_{\text{tran},e} = P_{\text{cond},e} + P_{\text{conv},e}$ and the total loss power from the electrons is $P_{\text{loss},e} = P_{\text{tran},e} + P_{0,\text{ion}} + P_{\text{Rad}}$, where $P_{0,\text{ion}}$ is the ionisation loss power and P_{Rad} the radiated power. The total transport loss power through both channels is then $P_{\text{tran}} = P_{\text{tran},e} + P_{\text{tran},i}$.

2.2.1. Results of power balance analysis. Results from the interpretive, power balance analysis of the high-power 3.5 MA pulse #94 980 with the high gas fuelling rate ($\Gamma_{D2} \sim 2.3 \times 10^{22} \text{ e s}^{-1}$) are shown in figure 3. The derived profiles are shown averaged over the period 10–12 s of the ELMy H-mode phase, while the measured raw data in figure 3(a) is shown at 11.1 s.

Components of the radially-integrated ion and electron power balances are shown in figures 3(b) and (c). While T_i only slightly exceeds T_e across the full plasma radius, collisional exchange transfers significant power from the ions to the electrons, i.e. integrated out the pedestal top $P_{ie} \sim 6$ MW, i.e. about $\sim 50\%$ of the total ion heating $P_{\text{heat},i}$. Consequently, at the pedestal top, similar powers are conducted through the electron and ion channels, with $P_{\text{tran},e} \sim P_{\text{tran},i} \sim 10$ MW, in spite of the fact that at mid-radius the integrated power heating and conducted by the ions are twice those in the electron channel. Almost half of the total loss power through the electron channel $P_{\text{loss},e}$ is radiated, i.e. $P_{\text{Rad}}/P_{\text{loss},e} \sim 40\%$, predominantly by the strong W emission from the mantle region.

Note that on including the heavier ^3He ion species in the TORIC calculations, significant ICRH power is deposited to the D^+ ions, with a ratio of on-axis power densities in (MW m^{-3}) of $Q_{i,\text{RF}}/Q_{e,\text{RF}} \sim 0.15/0.04 \sim 3$, while (wrongly) assuming instead a single H (3%) minority species results in insignificant core ion heating).

Results from the interpretive, power balance analysis of the high-power 3.5 MA pulse #96 713 with the lower gas fuelling rate ($\Gamma_{D2,\text{gas}} \sim 1.0 \times 10^{22} \text{ e s}^{-1}$) and the $f_{\text{Pel}} \sim 45$ Hz

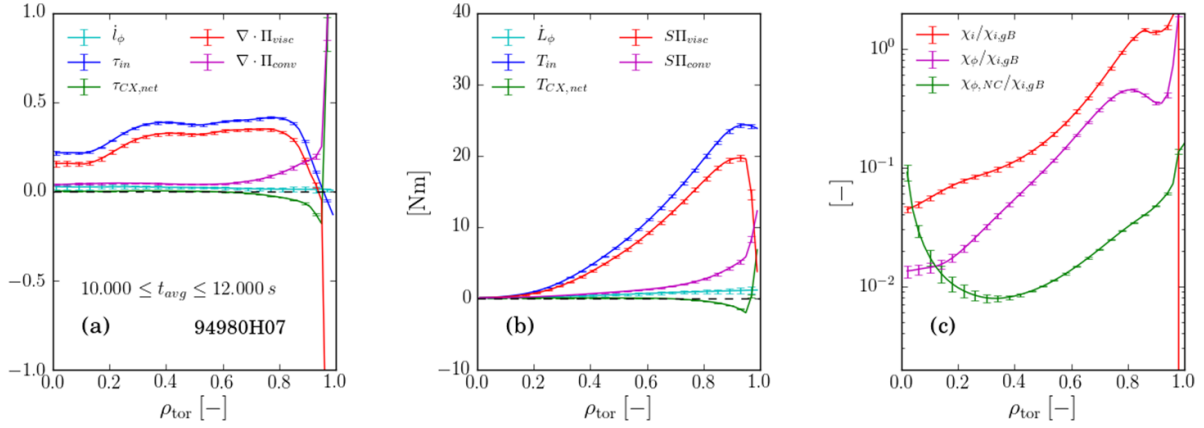


Figure 5. Results of interpretive, momentum balance analysis using TRANSP of pulse #94 980 showing: (a) input and net CX torque densities τ_{in} and $\tau_{CX,net}$, rate of change of angular momentum \dot{L}_ϕ and divergences of viscous and convected momentum fluxes $\nabla \cdot \Pi_{visc}$ and $\nabla \cdot \Pi_{conv}$; (b) the quantities shown in (a) volume integrated out to radius ρ_{tor} ; (c) the ion thermal and momentum diffusivities, normalised to the ion-gyro-Bohm thermal diffusivity, i.e. $\chi_i/\chi_{i,gB}$ and $\chi_\phi/\chi_{i,gB}$, where the TRANSP profiles are averaged over the sustained ELMy H-mode phase ($10.0 \leq t \leq 12.0$ s).

ELM-pacing pellets, with a similar total fuelling rate as pulse #94 980 are shown in figure 4.

The most striking difference between the kinetic profiles for these two pulses is the much higher (~ 2) toroidal rotation rate of $\Omega_{\phi,0} \lesssim 130 \text{ krad s}^{-1}$ in pulse #96 713, cf $\sim 70 \text{ krad s}^{-1}$ in pulse #94 980. Also, there is a higher ratio of $T_i/T_e \sim 1.3$ across the core plasma. Quoting values at the pedestal top, the exchange heating $P_{ie} \sim 9 \text{ MW}$ transfers $\sim 50\%$ of the total ion heating $P_{heat,i} \sim 18 \text{ MW}$ to the electrons. In fact, the exchange heating of the electrons P_{ei} almost equals that from the external electron heating $P_{heat,e} \sim 11 \text{ MW}$ and equals the radiated power from the electrons P_{Rad} .

Hence, accounting for the ion-electron exchange power and radiation, the net transport loss power through the ion channel $P_{tran,i} \sim 12 \text{ MW}$ is similar in magnitude to that transported through the electron channel $P_{tran,e} \sim 11 \text{ MW}$. The increased radiation in #96 713 ensures that about 50% of the total electron loss power $P_{loss,e} \sim 20 \text{ MW}$ through the electron channel is lost by radiation (again quoting values at the pedestal top).

In both pulses, the profiles of power deposition density to the ions and electrons differ in that, whereas $Q_{i,heat}$ peaks on-axis, $Q_{e,heat}$ peaks in the mantle region. This is because the fraction of NBI power heating the ions ($Q_{NB,i}/(Q_{NB,i} + Q_{NB,e})$) increases with the ratio of T_e to the injection energy E_0 , with $Q_{NB,e}/Q_{NB,i} > 1$ for $E_0/T_e > 15$. Consequently, the ratio of heating power to the ions relative to that to the electrons P_i/P_e is higher and also more peaked in #96 713 in which $T_i/T_e > 1$ than in pulse #94 980, i.e. $P_i/P_e \sim 1.33$ cf ~ 1.18 . In spite of the fact that this pulse has only H (1%) minority ions, more ICRH power is deposited into the D^+ ions than into the electrons, with a ratio of on-axis power densities in (MW m^{-3}) of $Q_{i,RF}/Q_{e,RF} \sim 1.1/0.4 \sim 2.8$.

The cause of the more peaked power deposition and greater fraction of ion heating in pulse #96 713 with the pellet+gas

fuelling is partly the increased density peaking $\bar{n}_e/n_{e,ped}$, mentioned in section 2.1. This, together with the higher overall heating power $\sim \times 1.15$ in this pulse compared to that in pulse #94 980 results in higher rotational shear and a higher T_i/T_e ratio. Because of the relatively higher radiated power in pulse #96 713, the ratio of ion to electron heat fluxes q_i/q_e is close to unity at the pedestal top in both pulses. Transport in these two pulses are compared in section 2.3, revealing modest differences in the heat and momentum diffusivities and hence changes to the prevailing transport mechanisms induced by the difference in fuelling method.

2.2.2. Results of momentum balance analysis. Results of the interpretive toroidal angular momentum balance analysis using TRANSP for the same two high-power, 3.5 MA pulses #94 980 and #96 713 are shown in figures 5 and 6. Torque densities τ (Nm m^{-3}) are shown in (a), radially integrated torques T (Nm) in (b) and gyro-Bohm normalised momentum and ion heat diffusivities in (c).

The dominant source of input torque $T_{\phi,in} \sim 25\text{--}30 \text{ Nm}$ is from the NBI heating. Note that because of the more peaked density profile in pulse #96 713, the torque density profile $\tau_{\phi,in}$ is somewhat more peaked than in pulse #94 980, which is partly responsible for the increased toroidal rotation rate. Note that in both pulses, the rate of change of angular momentum \dot{L}_ϕ is small, i.e. there is a steady rate of toroidal rotation during the averaging period.

In the gas-fuelled pulse #94 980, in which $T_i \sim T_e$, the momentum and ion diffusivities are very similar, i.e. the Prandtl number $Pr = \chi_\phi/\chi_i \sim 1$ except near the pedestal top. Except in the very core, both the ion thermal and momentum diffusivities are much larger than the ion-NC level, i.e. $\chi_i/\chi_{i,NC}$ and $\chi_\phi/\chi_{i,NC} \sim \mathcal{O}(10)$ across the plasma.

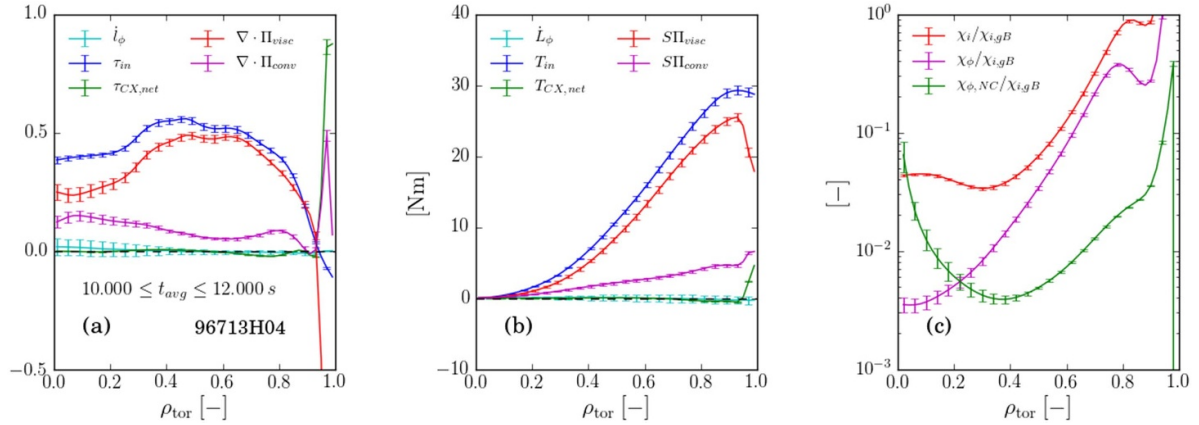


Figure 6. Results of interpretive, momentum balance analysis using TRANSP of pulse #96713, where the TRANSP profiles are averaged over the sustained ELMy H-mode phase ($10.0 \leq t \leq 12.0$ s). The definition of the quantities plotted are the same as in figure 5.

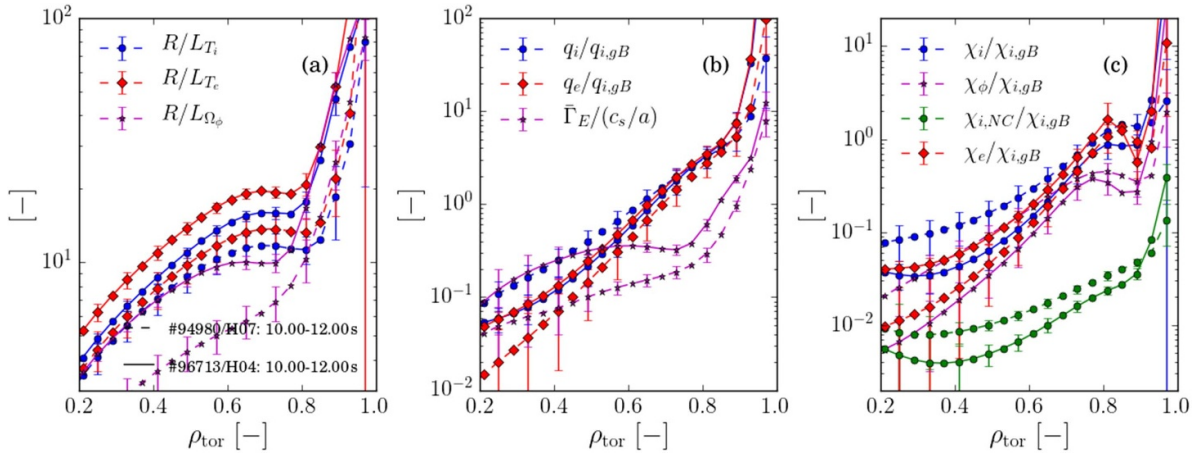


Figure 7. Results of interpretive, TRANSP power balance analyses of JET-ILW pulses #94980 (dashed) and #96713 (solid) showing time-averaged profiles over the ELMy H-mode phase of: (a) the normalised gradients R/L_{T_e} (◆) and R/L_{T_i} (●) and of toroidal rotation R/L_{Ω_ϕ} (★); (b) the electron and ion heat fluxes $q_e/q_{i,gB}$ (◆) and $q_i/q_{i,gB}$ (●) normalised to the ion gyro-Bohm level $q_{i,gB}$ and the normalised $E \times B$ shearing rate $\bar{\Gamma}_E = \gamma_E/(c_s/a)$ (c_s is the sound speed) (★); and (c) thermal diffusivities of the electrons $\chi_e/\chi_{i,gB}$ (◆), ions $\chi_i/\chi_{i,gB}$ (●) and the ion neo-classical diffusivity $\chi_{i,NC}/\chi_{i,gB}$, all normalised to the ion-gyro-Bohm thermal diffusivity $\chi_{i,gB}$.

As discussed further in section 2.3, in pulse #96713 with the pellet + gas fuelling, the ion thermal diffusivity is slightly less than that for the electrons, $\chi_i/\chi_e \sim 0.8$, both remaining $\sim \mathcal{O}(10)\chi_{i,NC}$. However, there is a more significant reduction in χ_ϕ , with the Prandtl number below $Pr \lesssim 0.5$, particularly further into the core.

In the pedestal region, CX collisions with cold neutral D^0 atoms results in a radially-integrated, frictional torque $T_{\phi,CX(net)} \sim \mathcal{O}(10)$ Nm, which opposes the torque imposed by the NBI. This torque $T_{\phi,CX(net)}$ is $\sim \times 1.5$ (and $\tau_{\phi,CX(net)} \sim \times 3$) higher in the gas-fuelled pulse #94980 than in the pellet + gas fuelled pulse #96713, primarily because the D^0 influx at the LFS is higher in the gas fuelled pulse.

The large CX torque density ($\tau_{\phi,CX(net)} \sim \mathcal{O}(1)$ Nm $^{-2}$) necessitates a large negative viscous momentum flux $\Pi_{\phi,visc}$ across the pedestal to achieve momentum balance. This implies the presence of a strong momentum ‘pinch’ that can arise from neo-classical effects [37] and/or be driven by turbulence [38]. While the presence of this momentum pinch is

worthy of more detailed study, it is beyond the scope of this paper.

2.3. Comparison of core heat and momentum transport in pulses #94980 and #96713

The time-dependent, interpretive TRANSP analysis solves the balance equations for the transport of particles, ion and electron heat and toroidal momentum [24, 39]. The source of kinetic profiles (T , n_e , T_i , Ω_ϕ and $\langle \epsilon_{tot} \rangle$) and other input data, the magnetic equilibrium used for mapping the profiles onto normalised radius ρ_{tor} and other assumptions in setting up the runs, e.g. on the impurity densities, are described in detail in section 2.2.

A comparison of results from the solution of the power balances of the ions and electrons and of toroidal momentum are shown in figure 7 for the pulses #94980 with gas-fuelling alone and #96713 with pellet + gas fuelling, where the profile data is averaged over a 2 s period of the ELMy H-mode phase.

It can be seen from figure 7(a), that across the core plasma the normalised gradients R/L_{T_e} , R/L_{T_i} and R/L_{Ω_ϕ} are all larger in pulse #96 713 than in pulse #94 980, with R/L_{T_i} and $R/L_{T_e} \sim \times 1.5$ higher and $R/L_{\Omega_\phi} \sim \times 2$ higher at mid-radius. This increase is a signature of improved energy and momentum confinement, particularly in the ion channel across the core plasma in the pellet + gas fuelled pulse.

The heat fluxes in the ion and electron channels $q_i/q_{i,gB}$ and $q_e/q_{e,gB}$, normalised to the ion-gyro-Bohm heat flux $q_{i,gB}$ are plotted in figure 7(b)¹⁴. For pulse #96 713 with gas + pellet fuelling, these normalised heat fluxes are almost equal with $q_i \sim q_e$ right across the core plasma. In contrast, for the gas fuelled pulse #94 980, while $q_i \sim q_e$ in the mantle region ($0.7 \leq \rho_{tor} \leq 1$), deeper into the core plasma q_i progressively exceeds q_e , with $q_i/q_e \gtrsim 10$ in the core.

The normalised, perpendicular $E \times B$ shearing rate $\bar{\gamma}_E = \gamma_E/(c_s/a)$ ¹⁵, also shown in figure 7(b), is considerably higher in pulse #96 713 than in pulse #94 980, by up to a factor ~ 3 at mid-radius. This shearing can suppress the amplitude of ion-scale turbulence when $\bar{\gamma}_E \gtrsim \mathcal{O}(1)$ [41, 42], thereby reducing the associated heat flux. Hence, it is likely that $E \times B$ shear plays a more significant role in regulating the level of turbulent ion heat transport in pulse #96 713, in which $\bar{\gamma}_E \lesssim 0.3$ at mid-radius, than in pulse #94 980.

Thermal diffusivities for the ion and electron channels, normalised to the ion-gyro-Bohm thermal diffusivity, $\chi_i/\chi_{i,gB}$ and $\chi_e/\chi_{e,gB}$ are compared in figure 7(c) for the same two pulses, together with the normalised diffusivity of the toroidal angular momentum $\chi_\phi/\chi_{i,gB}$. Also shown is an estimate of the gyro-Bohm normalised, neo-classical (NC) ion thermal diffusivity $\chi_{i,NC}/\chi_{i,gB}$, which is calculated in TRANSP using the NCLASS code [43].

It can be seen from figure 7(c) that for both pulses, in the peripheral mantle region the normalised thermal diffusivities of the ions and electrons are approximately equal, i.e. $\chi_i/\chi_e \sim 1$. For pellet + gas fuelled pulse #96 713 this is also the case right across the core plasma. In contrast, for the gas fuelled pulse #94 980, further into the plasma χ_i progressively exceeds χ_e , with $\chi_i/\chi_e \gtrsim 10$ in the core. In both pulses these thermal diffusivities far exceed the ion neo-classical level, with both $\chi_{i,e}/\chi_{i,NC} \sim \mathcal{O}(10)$. This certainly indicates that ion-scale turbulent transport is by no means fully suppressed in either pulse.

In both pulses, the Prandtl number $Pr = \chi_\phi/\chi_i$ decreases from $Pr \sim 0.5$ at $\rho_{tor} \sim 0.7$ both deeper into the core plasma and outward across the pedestal region, which is an indication that there is some degree of suppression of ion-scale turbulence (which results in stronger viscosity than electron scale turbulence) in the core and peripheral regions.

These results suggest that ion-scale turbulence (ITG or TEM), which can result in both ion and electron heat transport with equal efficacy, is primarily responsible for the core heat

transport in both pulses. However, in the higher performance pulse #96 713 with pellet + gas fuelling, at least some of the increased ion pressure in the core may be caused by a modest relative reduction in the efficiency of ion-scale, turbulent heat transport, caused by the increased $E \times B$ flow shear across the core plasma.

In spite of the fact that in both pulses the integrated heating power to the ions is approximately equal at mid-radius, the $\sim \times 3$ higher χ_i in the gas fuelled pulse #94 980 results in lower core T_i gradient and hence reduced core ion energy confinement than in the pellet + gas fuelled pulse #96 713. This is a consequence of the more peaked ion heating and torque deposition profiles resulting from the reduced pedestal density with the pellet + gas fuelling compared to that with the gas fuelling alone.

2.4. W impurity behaviour in 3.5 MA baseline pulses

In high-power ITER-baseline scenario pulses with $\gtrsim 25$ MW of heating power, a substantial fraction of the input power is radiated from the core plasma, i.e. $\mathcal{F}_{Rad} \sim 30\% - 40\%$. It has been shown in [8] that these losses are dominated by radiation from W impurities, which accounts for $\gtrsim 95\%$ of the total radiation. In such pulses, these impurities are typically localised to the outer ‘mantle’ region of the confined plasma, e.g. as shown for the 3 MA/2.8 T pulse #92 432 with 32 MW heating power in figure 13(a). The radially outward centrifugal force due to the toroidal rotation localises the heavy W ions to the LFS mid-plane where the total emissivity ϵ_m peaks [44]. However, because of the very high parallel electron thermal conductivity $\chi_{e,\parallel} \gg \chi_e$, it is the flux-surface-averaged emissivity $\langle \epsilon_{tot} \rangle$ that is relevant to the electron power balance (see figure 2(b)).

The reason why the impurity ions tend to remain localised to the mantle region in these ITER-baseline pulses is because the density gradient across the core plasma is much weaker than that of the ion temperature, i.e. there is a low degree of density peaking. As is discussed in [8] and references therein, the radial neo-classical convection velocity of impurity ions is proportional to the parameter $\zeta_{NC} = R/2L_{T_i} - R/L_{n_i}$ [45]. Hence, a *peaked* T_i profile and a *flat* n_e profile favours outward neo-classical convection, expelling the impurities from the plasma core. The converse is also true and, particularly in ‘hybrid’ scenario plasmas [1], which operate with a lower pedestal density $n_{e,ped}$ and consequently with a more peaked n_e profile, this can cause the W impurities to accumulate in the plasma core and lead to radiation collapse.

The evolution of the flux-surface-averaged W impurity density $\langle n_W \rangle$ is shown in figures 8(a)–(c) for the three 3.5 MA ITER-baseline pulses discussed in section 2, from which it can be seen that the W is typically localised to the mantle region, i.e. $0.7 \leq \rho_{tor} \leq 1$. Only in one of these pulses #94 980 is there a brief period during which $\langle n_W \rangle$ peaks in the plasma core but these impurities are expelled again later.

Also shown in figures 8(d)–(f) is a comparison of the evolution of profiles of the neo-classical convection parameter ζ_{NC} . This is calculated from the results of an interpretive TRANSP calculation, which is based on kinetic data provided from fits

¹⁴ The ion gyro-Bohm heat flux is defined here as $q_{i,gB} = -n_i \chi_{i,gB} T'_i$, where the associated heat diffusivity $\chi_{i,gB} = v_{th,i} \rho_i^2 / L_{T_i}$ and $v_{th,i} = \sqrt{2T_i/m_i}$ [21, 40].

¹⁵ The parameter c_s/a , where c_s is the sound speed and a the minor radius, is an estimate for the typical growth rate γ_{lin} of ion-scale turbulence [40].

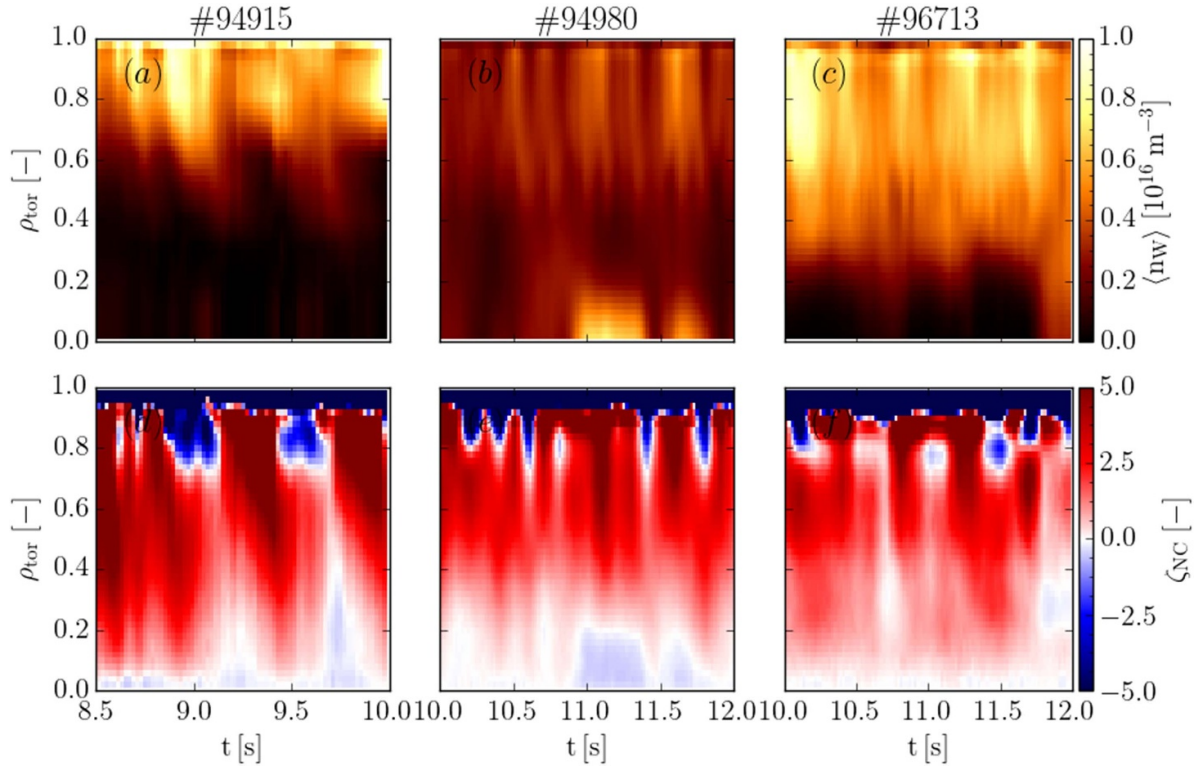


Figure 8. Comparison for the three 3.5 MA/3.3 T ITER-baseline scenario pulses with different fuelling #94 915 (a, d), #94 980 (b, e) and #96 713 (c, f) shown in figure 1 of: (a)–(c) the flux-surface-averaged W impurity density $\langle n_W \rangle$ (top); and (d)–(f) the neo-classical convection parameter ζ_{NC} (bottom), both as a function of ρ_{tor} . For #94 980 and #96 713 the W density is determined from the integrated analysis of [34], while for #94 915 it is determined by assuming W radiation dominates the total emissivity from bolometer tomography, i.e. that $\langle n_W \rangle = \langle \epsilon_{tot} \rangle / (n_e \mathcal{R}_e)$, where $\mathcal{R}_e \sim 4.5 \times 10^{-13} \text{ W m}^3$ is the total emissivity coefficient of W in the mantle region.

to electron density n_e and temperature T_e profile data measured by the HRTS [29] and Ne^{10+} impurity ion temperature T_i and toroidal rotation Ω_ϕ profile data from the core and edge CXRS systems [30].

From these plots it can be seen that, while $\zeta_{NC} \sim \mathcal{O}(-100)$ is strongly negative in the pedestal region (off the colour scale), hence driving the impurities across the pedestal into the confined plasma, it is weakly positive $\zeta_{NC} \gtrsim 5$ right across the core of the plasma. Consequently, once inside the confined plasma, the impurities are screened from the core plasma by outward convection, which concentrates them in the outer mantle region. Note that the convection velocity $V_{NC} \propto Zq^2 D_c \zeta_{NC} / R$, where Z is the impurity ion charge and D_c is the collisional diffusivity [45]. Typically, the W ions are in charge states W^{25-30+} in the mantle region (see figure 9(c)), so this convection is very strong for the W ions. Also, the strong poloidal asymmetry enhances the convection by a further factor $1/(2 \varepsilon^2) \sim 5$, where the inverse aspect ratio $\varepsilon = r/a$ [46].

Note that there are circumstances in these high-power, ITER-baseline pulses in which profile changes following an H- to L-mode transition, triggered by the strong W radiation from the plasma periphery, causes a sudden accumulation of the impurities. This typically leads to termination of the high-performance phase, either triggering a ‘pulse stop’ or causing a disruption due to radiation collapse. Such a radiation event occurs in the 3 MA pulse #92 432, the phenomenology of which is described in section 2.6.

Note that in pulse #94 915, during the periods of ELM-free H*-mode¹⁶, radiative cooling of the mantle region by the increasingly strong W radiation together with a concomitant increase in density, causes stronger outward convection ($\zeta_{NC} \gg 0$), localising the W to the plasma periphery. However, during the subsequent periods with rapid type-III ELMs, the resulting increase in the n_e gradient in the mantle causes this convection to reverse ($\zeta_{NC} < 0$), thereby allowing the W impurities to penetrate deeper in to the plasma, although they do not accumulate in the core.

While the W impurities are localised to the mantle region by the outward neo-classical convection, they can be efficiently expelled from the confined plasma by the ELMs. The ELMs typically expel a small fraction of the plasma particles, peeling off part of the edge plasma, causing relative density losses $\Delta \bar{n}_e / \bar{n}_e \sim 5\%–10\%$. If the impurities are concentrated in the periphery, the ELMs can ‘flush’ out a larger relative fraction of the impurity content than that of the main ions.

We define here the flushing efficiency of the W impurities by an ELM as $(\Delta \bar{n}_W / \bar{n}_W)_{ELM}$, i.e. the relative change in the W content of the plasma due to the ELM. Because the total radiation in high-power, JET-ILW pulses is dominated by that from W, this flushing efficiency can be evaluated

¹⁶ Here, the notation H* is used to refer to ELM-free H-mode rather than ELMy H-mode.

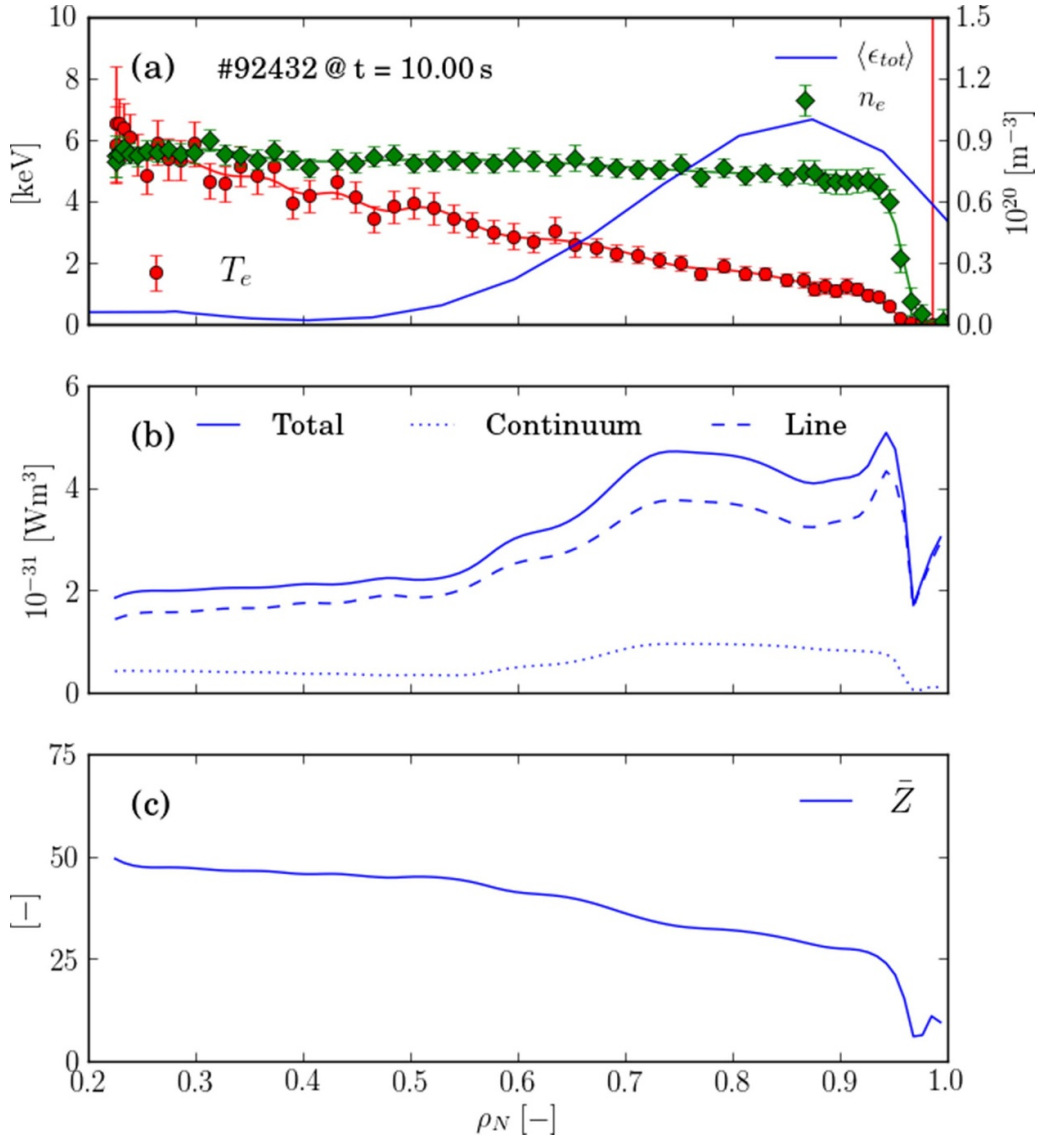


Figure 9. Profiles for the high-power, JET-ILW pulse #92 432 at 10 s of: (a) electron temperature T_e (●) and density n_e (◆) measured by high-resolution Thomson scattering and flux-surface averaged, total emissivity $\langle \epsilon_{tot} \rangle$ from bolometer tomography (solid-blue); (b) emissivity coefficients \mathcal{R}_e for W radiation (total-solid, line-dashed and continuum-dotted) from ADAS [48, 49]; and (c) mean ionic charge \bar{Z} of W, where coronal ionisation balance is assumed for the W atomic data.

from fast, bolometric measurements of the total radiation from the confined plasma, as described in detail in the following section 2.5.

2.5. Evaluation of ELM W ‘flushing’ efficiency

An estimate of the efficacy of each ELM at flushing the W impurities from the confined plasma (and also their influx during the inter-ELM periods) can be obtained from an analysis of fast, bolometric total radiation measurements, using a method first applied to JET-ILW plasmas described in [47]. For this analysis we use a fast radiated power signal P_{Rad}^{Hor} calculated from a weighted sum of intensities from a bolometer camera viewing the main chamber horizontally from the LFS [28].

As shown in figure 9(b) for the high-power, 3 MA ITER-baseline pulse #92 432, the total emissivity coefficient of W

is reasonably constant over the mantle region ($0.7 \leq \rho_N \leq \rho_{N,ped} \sim 0.96$), i.e. $\mathcal{R}_e \sim 4.5 \times 10^{-31} \text{ MW m}^{-3}$, where the W radiates most intensely (see figure 9(a)). Typically, in the mantle region, where $T_e \sim 1\text{--}3 \text{ keV}$, the average charge state \bar{Z} of the impurities is W^{25-30+} . The atomic data shown in figure 9 is from the ADAS database of spectroscopic data [48] and uses total radiated line power (\mathcal{P}_{LT}) data for W from [49].

As the W radiates mainly from the mantle region and the emissivity of W is reasonably constant over the relevant temperature range (1–3 keV), the average W density \bar{n}_W in the mantle can be estimated from the expression: $\bar{n}_W \sim P_{Rad}^{man} / (\bar{n}_e \mathcal{R}_e V_{man})$, where \bar{n}_e is the average density over the mantle region and V_{man} is the volume of the mantle $\sim 22 \text{ m}^3$. We next explain how we obtain a fast enough signal P_{Rad}^{man} quantifying the radiated power from the mantle region to

determine the ELM flushing efficiency, which requires a frequency response of order 1 kHz.

The power radiated from the confined plasma P_{Rad}^{Pl} can be calculated from a weighted sum of horizontally viewing, line-integrated measurements of total intensity measured using a multi-chord bolometer system [28]. This system has a sample rate of 5 kHz and uses an adaptive filtering algorithm so as not to smooth fast transients due to ELMs, while having lower bandwidth of typically 0.2 kHz during steady phases. As this calculation relies on assumptions on the symmetry of the emissivity on flux surfaces, it tends to overestimate P_{Rad}^{Pl} by as much as 50% in the presence of highly in-out asymmetric emissivity distributions. Here, we refer to this fast radiated power signal as P_{Rad}^{Hor} .

In order to overcome this problem and accurately calculate the radiated power from the mantle region P_{Rad}^{man} , we use the total emissivity distribution $\varepsilon_m(R, z)$ obtained from tomographic inversion [27] of the multi-chord bolometer data, which take proper account of the poloidal asymmetry. Reconstructions are calculated at the mid-times of each inter-ELM period, using input data averaged over 5 ms intervals. The resulting distributions are integrated over the volume of the mantle to form a ‘slow’ radiated power signal we refer to here as $\langle P_{Rad}^{man} \rangle$. Note that in these high-power, ITER-baseline scenario pulses, typically $\sim 70\%$ of the radiated power is emitted from the mantle region (see figure 10(c)).

We can correct the fast radiated power signal P_{Rad}^{Hor} to provide a more accurate, fast estimate of P_{Rad}^{man} by scaling it to the more accurate, slow signal $\langle P_{Rad}^{man} \rangle$ obtained from the tomography using a time-dependent scale factor. While this procedure may seem complicated, it is necessary if we are to use the resulting values of P_{Rad}^{man} to estimate the concentration of W in the mantle region.

From both the fast estimate of the radiated power from the mantle P_{Rad}^{man} and a fast measurement of the line-average density \bar{n}_e from the lower, horizontal interferometer channel (#5), which passes through the outer half of the lower plasma cross-section, the ELM W flushing efficiency can be evaluated from the change in the signal $f_{fl} = P_{Rad}^{Hor} / \bar{n}_e$ aka the ‘flushing’ signal between short averaging periods just before and after the ELM crash, i.e. from the expression $\Delta n_W / n_W \sim (f_{fl}^{pre-ELM} - f_{fl}^{post-ELM}) / f_{fl}^{pre-ELM} = \Delta(f_{fl}) / f_{fl}^{pre-ELM}$.

For our analysis we use pre- and post averaging times of $\Delta t_{ELM} = \{-7, -2 \text{ ms}\}$ and $\{5, 10 \text{ ms}\}$ relative to the time t_{ELM} of the peak Be II intensity signal. The post-ELM time period is delayed by 5 ms to avoid the transient increase in radiation that is caused by the ELM-sputtered W influx before the ionisation balance has had time to recover. It is a general phenomenon that when a population of impurity ions has not yet reached coronal ionisation balance, they are able to radiate more efficiently than when in equilibrium [50].

A similar measure, estimating the relative change in the W content between the ELMs, i.e. the relative inter-ELM ingress or ‘fluence’ of W $(\Delta \bar{n}_W / \bar{n}_W)_{i-ELM}$ can be calculated from the difference between the post-ELM value of f_{fl} and that prior to the subsequent ELM, i.e. $(\Delta \bar{n}_W / \bar{n}_W)_{i-ELM} = (f_{fl}^{pre-ELM_{i+1}} -$

$f_{fl}^{post-ELM_i}) / f_{fl}^{post-ELM_i}$. These measures of the ELM W flushing efficiency $(\Delta \bar{n}_W / \bar{n}_W)_{ELM}$ and the relative, inter-ELM fluence $(\Delta \bar{n}_W / \bar{n}_W)_{i-ELM}$ can then be used to calculate net rates of change of the W impurity content, $\gamma_W = (d\bar{n}_W / dt) / \bar{n}_W$ from a time-dependent average, as described in appendix B of [51].

In the case of a group of rapid ELMs, with an inter-ELM period shorter than the pre- and post-ELM averaging times of $\{-7, 10 \text{ ms}\}$, it is only possible to determine the flushing for the group of ELMs, which we choose to split equally between the sub-ELMs, while the inter-ELM fluence is allocated to the last in the group. A property of this ad-hoc method of handling the compound ELMs does maintain valid, time-averaged flushing rates γ_W calculated from the $\Delta \bar{n}_W / \bar{n}_W$ data. Rates of change of the W content due to the ELM flushing γ_W^{ELM} and the inter-ELM influx γ_W^{i-ELM} are shown in figure 11(c) of section 2.7 below, together with the ‘net’ rate of change due to the balance between these competing fluences, i.e. $\gamma_W^{net} = \gamma_W^{ELM} - \gamma_W^{i-ELM}$.

By availing of fact that radiation from W dominates the radiated power and that the total emission rate coefficient \mathcal{R}_e of W over the 1–3 keV temperature range in the mantle region is almost constant $\sim 4.5 \times 10^{-31} \text{ W m}^3$, the average W concentration over the mantle region $\langle C_W \rangle_{man}$ can also be estimated from the expression: $\langle C_W \rangle_{man} \sim P_{Rad}^{man} / (V_{man} \mathcal{R}_e \bar{n}_e^2)$. Typically, $\langle C_W \rangle_{man} \sim 2\text{--}3 \times 10^{-4}$ in these plasmas, e.g. as shown in figure 10(a).

An example of the application of this ELM-flushing analysis to the the high-power, 3 MA ITER-baseline pulse #92 432 is presented in the following section section 2.6.

2.6. ELM W flushing and ‘radiation event’ in pulse #92 432

The evolution of the high-power, 3 MA/2.8 T ITER-baseline pulse #92 432 with 32 MW of additional heating power and gas fuelling only at a rate of $\Gamma_{D2} \sim 2.3 \times 10^{22} \text{ e s}^{-1}$, is shown in figure 10 both as an example of the application of the ELM W flushing analysis described above but also to illustrate the profound effect that the strong W radiation can have on the evolution of such high-power H-mode pulses in JET-ILW. Note that this 3 MA pulse has the same q_{95} and plasma configuration as the 3.5 MA pulses discussed here.

Provided the W impurities remain primarily in the outer, mantle region of the plasma, their effect on the core fusion performance is relatively benign and their radiation helps distribute the power exhaust over the vessel walls. For this situation to persist, two criteria must be satisfied: firstly, the ELMs must flush out enough of the W that crosses the separatrix between ELMs to maintain a constant impurity content; secondly, the T_e and n_e gradients in the mantle must stay aligned such that the impurity convection is directed outwards, i.e. $\langle \zeta_{NC} \rangle_{man} > 0$, so that the W impurities are screened from the plasma core.

During the early ELM phase of the pulse ($\lesssim 10 \text{ s}$) these conditions are fulfilled, however, later the ELM frequency slows and they then cease at $\sim 10.2 \text{ s}$. During the subsequent, ELM-free H*-phase, the density \bar{n}_e , W content ($\bar{n}_W \propto P_{Rad}^{man} / \bar{n}_e$)

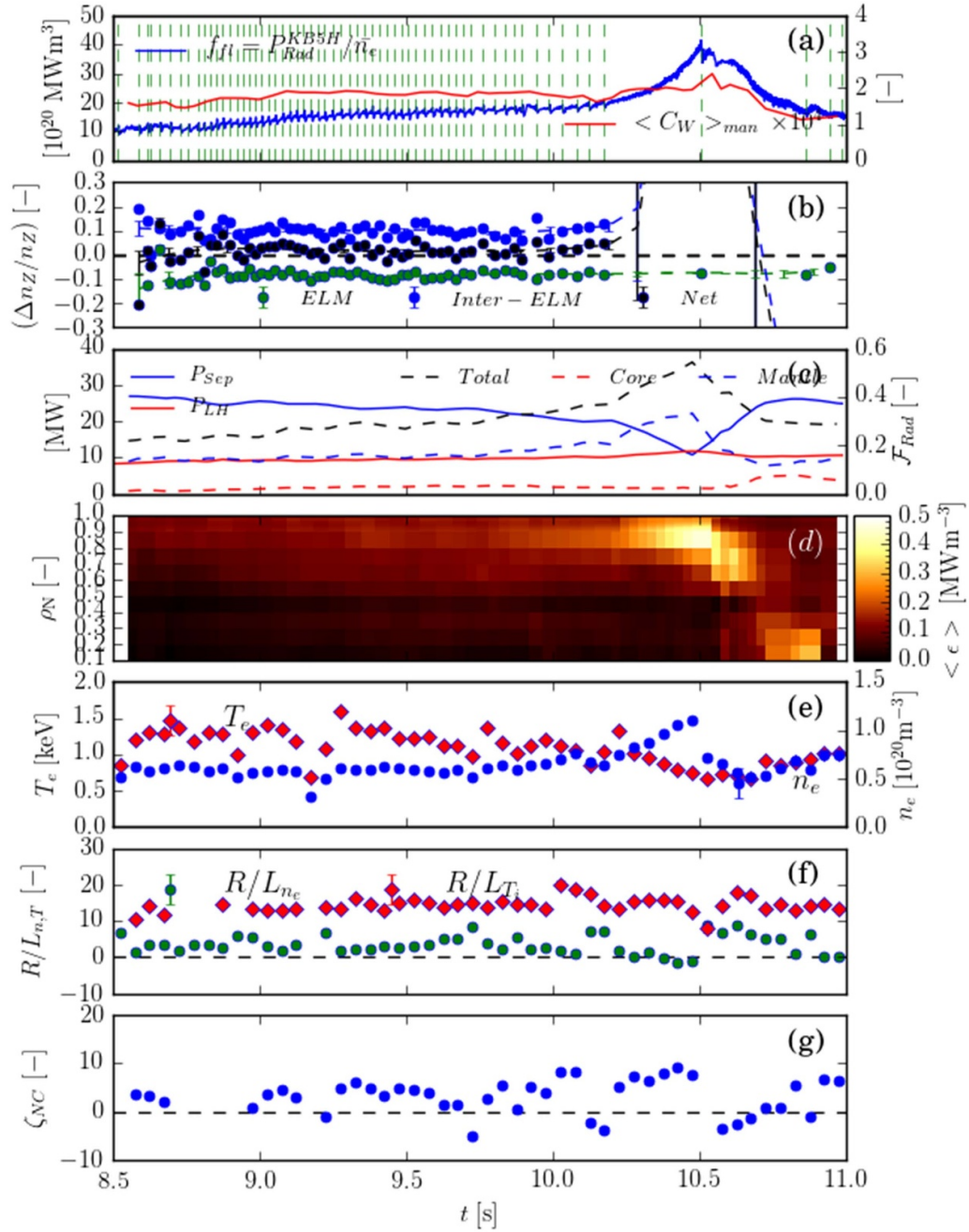


Figure 10. The evolution of JET-ILW pulse #92 432 illustrating the effect of W radiation on the mantle: (a) the signal $f_{fl} = P_{Rad}^{Hor}/\bar{n}_e$ (blue), the average W concentration in the mantle $\langle C_W \rangle_{man}$ (red) and the ELM times (green dashed); (b) the relative changes to the W content in the mantle $\Delta n_W/n_W$ caused by ELM flushing (green), the influx between ELMs (blue) and the net change over the ELM cycle (black); (c) the separatrix loss power $P_{Sep} = P_{in} - P_{Rad}^{Pl}$ (blue-solid) and the L/H-transition threshold power P_{LH} [52]; and the fractions of radiated power \mathcal{F}_{Rad} (RHS-dashed) from the confined plasma (black), the mantle (blue) and the core ($\rho_N \leq 0.5$) (red); (d) the flux-surface averaged emissivity $\langle \epsilon_m \rangle(\rho_N)$; (e) the electron temperature T_e (◆) and density n_e (●) at $\rho_N = 0.9$; and (f) the neo-classical convection parameter $\langle \zeta_{NC} \rangle_{man}$ averaged over the mantle region (blue).

and the associated radiation primarily from the mantle increase strongly, to a fraction $\mathcal{F}_{Rad} \gtrsim 70\%$ of the input power (see figure 10(c)). The slowing of the ELMs prior to the H*-phase is caused by an increase in the gas puffing rate by the control system, which is intended to increase f_{ELM} , i.e. this has the opposite effect to that expected. The phenomenology of these events is discussed further in section 3.

The consequent reduction of the net power crossing the separatrix $\Delta P_{Sep} = P_{l,th} - P_{Rad}^{Pl} - P_{LH}$ below L/H-transition

threshold power P_{LH} [52] triggers a subsequent back transition to L-mode (see figure 10(c)). Note that, the fact that P_{LH} increases with B_t means that this type of behaviour is more prone to occur in higher-current baseline-scenario pulses with higher B_t , making then more difficult to control.

As shown in figures 10(f) and (g), the resulting peaking of the n_e profile due to the loss of the density pedestal after the transition to L-mode results in a sudden reduction of the

neo-classical screening ($\zeta_{NC} \rightarrow 0$). As is evident from the evolution of the total emissivity $\langle \epsilon_{tot} \rangle$ shown in figure 10(d) this reduction in screening then causes sudden accumulation of the W impurities the plasma core, resulting in a reduction of the stored energy W_{pl} by $\sim 30\%$.

The influence of the strong mantle radiation on the electron power balance is evident from figure 10(e), which shows that there is a significant reduction of T_e just inside the pedestal top (at $\rho_{tor} = 0.9$) and a corresponding increase of n_e as the level of mantle radiation increases (see [8] for a detailed discussion of the electron and ion power balance in this pulse).

The resulting changes to the n_e and T_e gradients in the mantle initially causes $\langle \zeta_{NC} \rangle_{man}$ to increase (see figure 10(f)), driving the impurities more strongly outwards. At the H/L-transition at 10.5 s, $\langle \zeta_{NC} \rangle_{man}$ suddenly decreases to ~ 0 , when the normalised density gradient R/L_{n_e} in the mantle region steepens, causing the W impurities to rush into the plasma core. This behaviour is evident from the evolution of the total emissivity distribution $\langle \epsilon_{tot} \rangle$, which is shown in figure 10(d).

During the ELMy H-mode phase, as shown in figure 10(a), while the W concentration in the mantle ($\langle C_W \rangle_{man} \sim P_{Rad}^{man}/(V_{man} R_e \bar{n}_e^2)$) remains quite constant at $\langle C_W \rangle_{man} \sim 2 \times 10^{-4}$, there is a gradual increase in the W content $\bar{n}_W \propto P_{Rad}^{man}/\bar{n}_e$, causing a concomitant increase in the mantle radiation P_{Rad}^{man} (see figure 10(c)). This gradual increase is a result of a delicate balance between the flushing of the W impurities by the ELMs from the confined plasma and their influx across the pedestal between the ELMs.

The relative W flushing efficiency $\Delta \bar{n}_W/\bar{n}_W$ and inter-ELM W fluence $(\Delta \bar{n}_W/\bar{n}_W)_{i-ELM}$ evaluated for each ELM are shown in figure 10(b), together with the net, relative change in the W content over each ELM cycle, i.e. $(\Delta \bar{n}_W/\bar{n}_W)_{net} = (\Delta \bar{n}_W/\bar{n}_W)_{ELM} - (\Delta \bar{n}_W/\bar{n}_W)_{i-ELM}$. It is evident that, while $\sim 5\% - 10\%$ of the W content is flushed by each ELM, a similar amount is convected across the pedestal from the SOL and re-enters the plasma between the ELMs. The small, net change results in a gradual change on a timescale $1/\gamma_W^{net} \sim \mathcal{O}(1 \text{ s})$.

In this pulse, ELMy H-mode does resume at the end of the period shown but the high-Z impurities remain in the plasma core and the stored energy does not fully recover to the level prior to the radiation event. The use of ELM-pacing pellets in such pulses alters the characteristics of the ELMs and allows the duration such high-performance, ITER-baseline pulses to be extended. The behaviour of 3.5 MA ITER-baseline, H-mode pulses with ELM pacing pellets is discussed in the following section section 2.7.

2.7. ELM flushing and W behaviour in 3.5 MA pulses

In this section, we investigate the ELM flushing and W behaviour in the three 3.5 MA ITER-baseline pulses with different gas and/or pellet fuelling that were discussed previously in section 2. Results of the ELM W flushing analysis for these pulses are presented in figure 11.

Considering first, the pulse #94915 with the lower rate of gas fuelling ($\Gamma_{D2,gas} \sim 1.5 \times 10^{22} \text{ es}^{-1}$) alone, we see that this pulse is non-stationary, exhibiting three H*-phases, during which the mantle W radiation increases, just as occurred

in pulse #92432, as described in section 2.6 above. The W concentration in the mantle $\langle C_W \rangle_{man} \sim 2 \times 10^{-4}$ is similar in both of these gas-only fuelled pulses.

The strong mantle radiation does not result in an H/L-transition as in pulse #92432, instead the H*-phase is terminated by a single large amplitude ELM, which is followed by a sustained burst of small, type-III ELMs (see figure 1(e)). During these phases, the n_e gradient in the mantle region increases, resulting in a reversal of the neo-classical convection from outward to inward, as shown in figure 11(e). This reversal allows the W to migrate deeper into the plasma core, as is evident from the evolution of the total emissivity shown in figure 11(f), however, the impurities do not accumulate in the plasma core.

The combined effect of the few, large and frequent, small ELMs does provide sufficient flushing of the W to maintain a reasonably constant W concentration. However, during the final H*-phase, a strong increase of the total radiated power P_{Rad}^{tot} triggered an early ‘pulse-stop’, which initiated an increase in the gas fuelling rate. During the ramp-down phase of this pulse, there was a disruption, resulting in vessel forces exceeding 350 T. This non-stationary nature of high-power, ITER-baseline pulses with a low rate of gas fuelling leads to a high fraction of pulses disrupting, which is clearly unacceptable.

Increasing the D₂ gas puffing rate, as in pulse #94980 ($\Gamma_{D2,gas} \sim 2.3 \times 10^{22} \text{ es}^{-1}$), provides a safe means of controlling the W impurity level, and thereby reducing the disruptivity, but at the cost of decreased energy confinement. The more frequent ELMs induced by the increased gas puffing flush out more W, significantly reducing the W concentration to $\langle n_W \rangle_{man} \sim 1 - 1.5 \times 10^{-4}$. Note, however, that there is a gradual buildup of the W content due to the increasing \bar{n}_e (see figure 11(a)). The W impurities are also not so well screened from the core because of the reduced core T_i and hence weaker R/L_{T_i} , resulting in the neo-classical convection parameter $\zeta_{NC} \sim 0$ in the mantle region.

Comparison of the pedestal parameters shown in figures 11(e) and (f), shows that the increased gas puffing in pulse #94980 does not significantly reduce $T_{e,ped}$, or indeed increase $n_{e,ped}$, compared to those in pulse #94915. There is, however, a significant reduction in toroidal rotation rate $\Omega_{\phi,ped}$ at the top of the density pedestal caused by the increased gas puffing rate in pulse #94980. In both pulses, the ion temperature $T_{i,ped}$, here defined as T_i at the top of the density pedestal¹⁷, is significantly higher ($\sim 20\%$) than $T_{e,ped}$.

As already discussed above, the use of ELM-pacing pellets in pulse #96713 allows the duration of the high-performance phase to be extended without degrading the energy confinement. The main beneficial effect of the pellets is to trigger regular ELMs under conditions which would otherwise result in ELM-free H*-phases, as occur in pulse #94915. This allows pulse #96713 to be run with an even lower gas puffing rate ($\Gamma_{D2,gas} \sim 1.0 \times 10^{22} \text{ es}^{-1}$) than that used in pulse

¹⁷ As the ion temperature from the edge CXRS system typically does not exhibit a clear ‘knee’ at the pedestal, we do not fit the profile with an $\text{mtanh}()$ function [32] as is done for the T_e profile but instead take the pedestal value of T_i to be that at the top of the n_e pedestal.

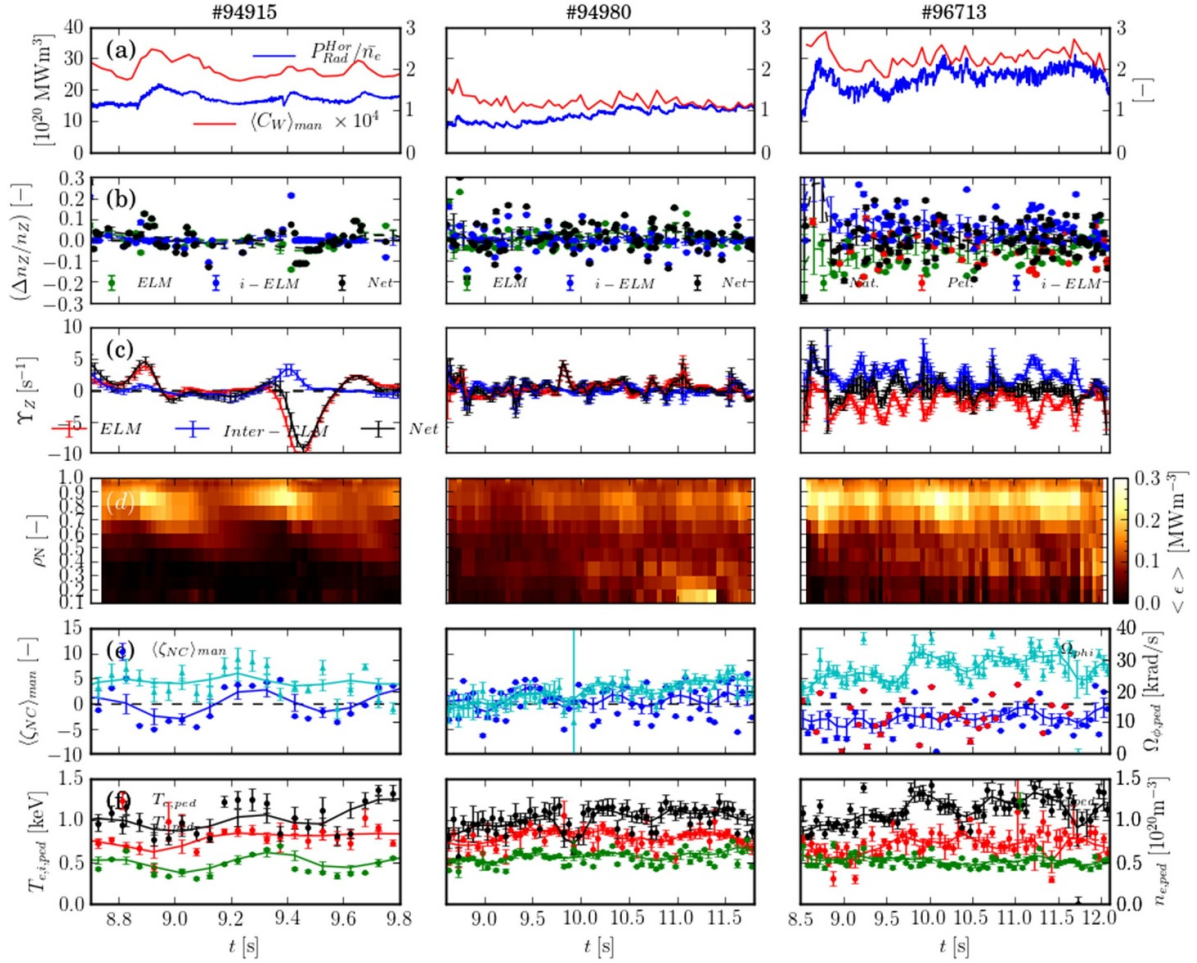


Figure 11. A comparison for the three high-power, 3.5 MA/3.3 T baseline-scenario JET-ILW pulses of figure 1 (key parameters given in table 1), showing the evolution of: (a) the signal $f_{fl} = P_{Rad}^{Hor}/\bar{n}_e$ (blue) and the estimated average W concentration over the mantle region $\langle C_W \rangle_{man}$ (red); (b) the fraction of W flushed per ELM $(\Delta \bar{n}_W/\bar{n}_W)_{ELM}$ for natural (●) and pellet-triggered (●) ELMs, the inter-ELM W influx $(\Delta \bar{n}_W/\bar{n}_W)_{i-ELM}$ (●) and the net fractional change in W content per ELM cycle (●); (c) the respective rates of change of the W content $\gamma_W = d(\Delta \bar{n}_W/\bar{n}_W)/dt$ due to the ELM flushing (γ_W^{ELM} —red), the inter-ELM influx (γ_W^{i-ELM} —blue) and the resulting net rate of change (γ_W^{net} —black); (d) the flux-surface-averaged total emissivity $\langle \epsilon_{tot} \rangle$ from bolometry; (e) the neo-classical convection parameter $\langle \zeta_{NC} \rangle_{man}$ averaged over the mantle region (blue and ●, ● following pellet-triggered ELMs) and the toroidal rotation rate $\Omega_{\phi,ped}$ (▲) measured by CXRS at the top of the density pedestal; and (f) the electron $T_{e,ped}$ (●) and ion $T_{i,ped}$ (●) pedestal temperatures and the pedestal density $n_{e,ped}$ (●).

#94 915 ($\sim 1.5 \times 10^{22} \text{ e s}^{-1}$). The danger with such a strategy is the necessity of reliable pellet injector operation to deliver a regular stream of pellets for the pulse to run without risk of a radiation induced disruption.

Although the total D_2 fuelling rate from gas and pellets, i.e. $\Gamma_{D2} \sim 2.3 \times 10^{22} \text{ e s}^{-1}$, is the same in pulse #96 713 as used in pulse #94 980, the performance of the pulse is superior in terms of its overall energy confinement. We will see that the origin of this lies not in significantly higher $T_{e,ped}$ but in increased toroidal rotation and hence rotational shear from the pedestal top, inwards across the core plasma and hence increased core ion energy confinement.

From figure 11(a), we can see that the W concentration of $\langle C_W \rangle_{man} \sim 2.5 \times 10^{-4}$ is in fact as high in pulse #96 713 as in pulse #94 915. As evident from the evolution of the total emissivity shown in figure 11(d), the W is also not as well screened from the plasma core as in pulse #94 915. Averaged over the mantle region, the neo-classical convection parameter is slightly negative $\langle \zeta_{NC} \rangle_{man} \sim -2$ in pulse #96 713,

i.e. weakly inwards (see figure 11(e)). However, the full radial profiles shown in figure 8(b), show that $\zeta_{NC} > 0$ at mid-radius, hence the N-C convection still acts to screen the W from the core.

Comparison of the pedestal parameters in figures 11(e) and (f), show that whereas $T_{e,ped}$ is similar in the three pulses, while $n_{e,ped}$ is slightly lower in the pulse #96 713 with the pellets, there is a significant difference in the ion parameters ($T_{i,ped}$ and $\Omega_{\phi,ped}$) from the edge CXRS measurements. In pulse #96 713, there is a greater ratio of $T_{i,ped}/T_{e,ped} \sim 1.6$, than in the other two pulses (~ 1.4) and the rotation at the pedestal top $\Omega_{\phi,ped}$ is also $\sim \times 1.4$ higher.

In section 2.1 above, we showed that this enhanced rotation in the pulse #96 713 with pellets and the lower rate of gas fuelling, in fact occurs right across the plasma from the pedestal to the core. This perhaps arises from reduced CX damping of the toroidal momentum due to the lower D^0 atomic density resulting from the reduced gas puffing into the main chamber.

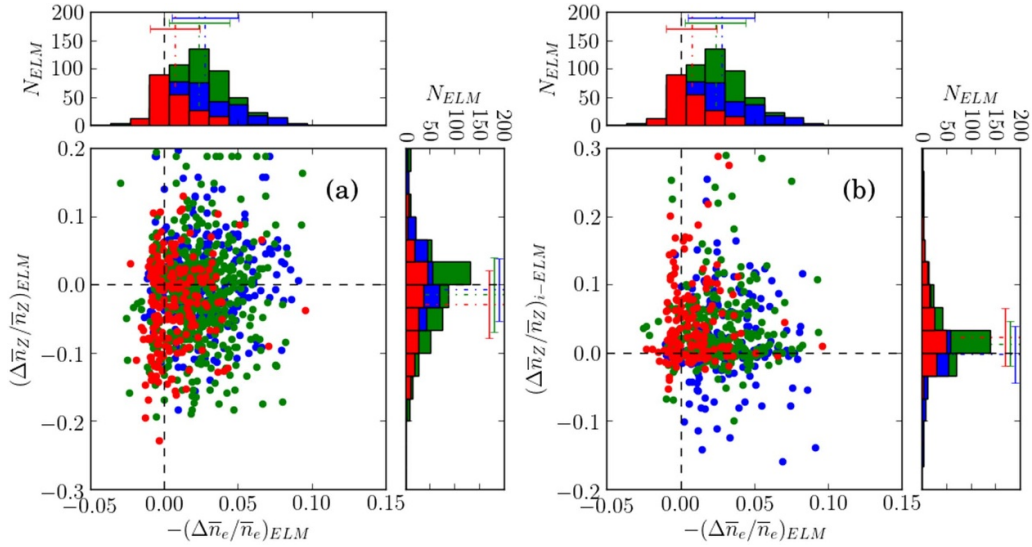


Figure 12. Comparison of data from six 3.5 MA/3.3 T baseline-scenario pulses with 30 – 37 MW of additional heating power with: only gas fuelling (#94 915 ($\Gamma_{D2} \sim 1.5 \times 10^{22} \text{ e s}^{-1}$), 94 964 ($3.0 \times 10^{22} \text{ e s}^{-1}$) and 94 980 ($2.3 \times 10^{22} \text{ e s}^{-1}$) •) and with both gas fuelling ($1\text{--}1.5 \times 10^{22} \text{ e s}^{-1}$) and pacing pellets ($f_{Pel} \sim 35 \text{ Hz}$) and (#96 536, 96 713 and 96 750 – •, •, for pellet triggered (•) and natural (•) ELMs, showing: (a) the relative change in W content of the confined plasma due to ELMs $(\Delta \bar{n}_z / \bar{n}_z)_{ELM}$ and (b) the inter-ELM fluences $(\Delta \bar{n}_z / \bar{n}_z)_{i-ELM}$. Histograms on the x- and y-axes show probability density functions (PDFs) of the respective quantities for the different ELM types: in gas-only pulses (•) and pulses with pacing pellets for natural (•) and pellet-triggered (•) ELMs), where the dashed lines and error bars represent the average values and standard deviations of the data points.

Table 5. Average values of data shown in figure 12 by fuelling source and ELM type for high-power, 3.5 MA/3.3 T ITER-baseline pulses.

Fuelling	ELM type	$\langle \Delta \bar{n}_e / \bar{n}_e \rangle$ (%)	$\langle \Delta \bar{n}_W / \bar{n}_W \rangle$ (%)	
		ELM	ELM	inter-ELM
Gas-only	Natural	-2.8 ± 0.1	-0.7 ± 0.3	0.2 ± 0.3
Pel and Gas		-2.4 ± 0.2	-1.4 ± 0.2	1.3 ± 0.2
	Pellet	-0.7 ± 0.1	-2.9 ± 0.4	2.3 ± 0.3
—	All	-2.2 ± 0.1	-1.4 ± 0.2	0.9 ± 0.2

In the following section section 2.8, the dependence of the W flushing efficiency $\Delta \bar{n}_W / \bar{n}_W$ on the fractional ELM density losses $\Delta \bar{n}_e / \bar{n}_e$ is investigated, classifying the data according to whether the ELMs are spontaneous or pellet-triggered events.

2.8. Influence of ELM type on W flushing efficiency

By identifying whether the ELMs are either spontaneous *aka* ‘natural’ or ‘pellet-triggered’ events, the data for the relative W flushing efficiency $(\Delta \bar{n}_W / \bar{n}_W)_{ELM}$ and inter-ELM fluence $(\Delta \bar{n}_W / \bar{n}_W)_{i-ELM}$ can be classified according to ELM type. This classification is performed by determining whether the occurrence of the ELMs is coincident with the arrival of the pellets at the plasma edge.

Such data is shown in figure 12 for six 3.5 MA baseline-scenario pulses with 30–37 MW of additional heating power, three with only D_2 gas fuelling at rates of $\Gamma_{D2, gas} \sim 1.5, 2.3$ and $3.0 \times 10^{22} \text{ e s}^{-1}$ and three with both gas fuelling ($1\text{--}1.5 \times 10^{22} \text{ e s}^{-1}$) and $\phi 2 \text{ mm}$ ELM pacing pellets ($f_{Pel} \sim 35 \text{ Hz}$). The W flushing $(\Delta \bar{n}_W / \bar{n}_W)_{ELM}$ and inter-ELM fluence $(\Delta \bar{n}_W / \bar{n}_W)_{i-ELM}$ data are plotted as a function of the relative ELM density losses $\Delta \bar{n}_e / \bar{n}_e$, which are determined from the decrease at the ELMs of the line-average density \bar{n}_e

from channel #5 of the FIR interferometer passing diagonally through the lower, outer half of the plasma cross-section.

To better quantify the differences in these parameters between the different classes of ELMs, histograms, i.e. PDFs, of the distributions of the data are plotted on the corresponding axis. These histogram plots also show the mean and standard deviation of the data for each class of ELMs. While the ‘natural’ ELMs typically result in density losses $\Delta \bar{n}_e / \bar{n}_e \sim 5\%\text{--}10\%$, the density losses due to pellet-triggered ELMs are smaller and some of the pellets result in a small net fuelling.

Note that these ELM-pacing pellets are smaller ($\sim 20\%$ of the particle content) than those used for fuelling, i.e. of $\phi 2 \text{ mm}$, see $\phi 4 \text{ mm}$ for the fuelling pellets, and are hence mostly ablated before reaching the pedestal top. Typical particle contents of the pacing and fuelling pellets are $\sim 4 \times 10^{20} \text{ e}^-$ and $\sim 2 \times 10^{21} \text{ e}^-$ respectively.

Average values and standard deviations of the data show in figure 12 are stated in table 5. For the natural ELMs, the average density losses $\langle \Delta \bar{n}_e / \bar{n}_e \rangle \sim -2.6 \pm 0.2\%$ are similar in both the gas-only and gas + pellet-fuelled pulses. However, for the pellet-triggered ELMs, on-average the density losses are considerably smaller $\langle \Delta \bar{n}_e / \bar{n}_e \rangle \sim -0.7 \pm 0.1\%$, i.e. there

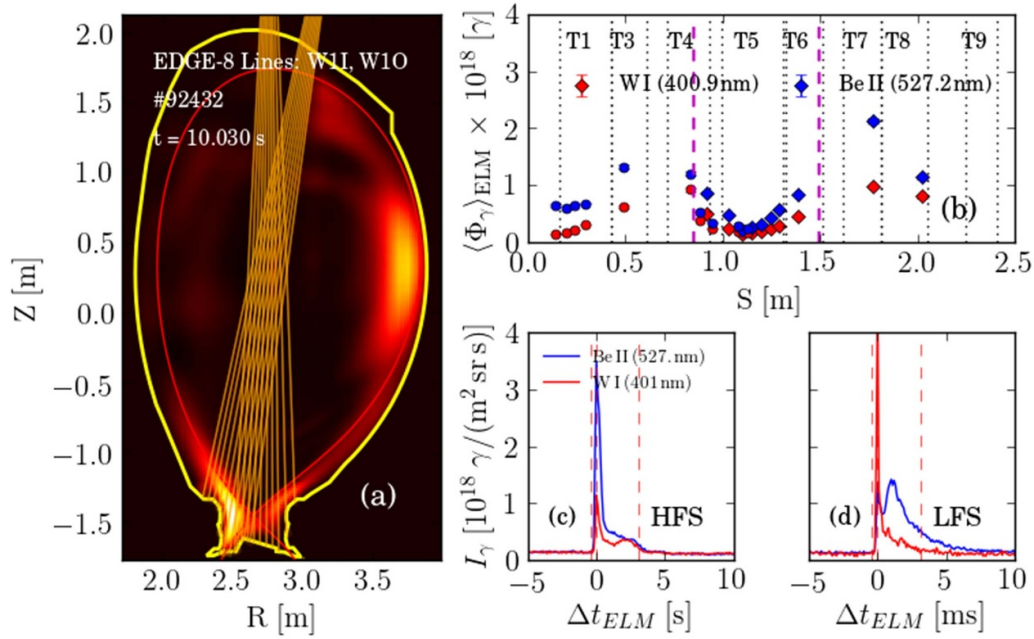


Figure 13. Bolometric total radiation and spectroscopic impurity influx data for the high-power, 3 MA JET-ILW pulse #92432 showing: (a) tomographic reconstruction of total emissivity $\varepsilon_m(R, z)$ at the peak of an ELM crash ($t = 10.035$ s) and lines of sight (LoS) of the multi-channel, visible range spectrometer system (KS3) viewing the divertor region (orange); (b) intra-ELM photon fluences $\langle \Phi_\gamma \rangle$ averaged over the period $8.5 \leq t \leq 11$ s of the WI (400.9 nm) and Be II (527.9 nm) lines vs the S-coordinate along the divertor target surface starting at the top corner of the inner ‘dome’ structure (the symbols indicate the LoS groups viewing the LFS (●) and HFS (◆) regions); and (c), (d) time evolution over a single ELM of the intensity of the same Be II and WI lines summed over the channels viewing the inner (c) and outer (d) divertor regions. In (a) and (b), the vertical lines indicate the locations of the strike points (magenta-dashed) and divertor tile edges (black-dotted).

is significant net fuelling of the confined plasma by many of the pacing pellets.

There is a large scatter in the ELM flushing $(\Delta \bar{n}_W / \bar{n}_W)_{ELM}$ and inter-ELM fluence $(\Delta \bar{n}_W / \bar{n}_W)_{i-ELM}$ data for several reasons. Firstly, the measurement method gives only an approximate measure and is prone to error. Also, while some ELMs are followed by ELM-free periods of significant duration, others are followed by the groups of rapid small ELMs, which complicates the measurement. In spite of these difficulties with the measurement, it may well be that some ELMs do result in a net *increase* in the W content as a result of an interchange component of the ELM instability [53], which could mix some cold plasma from the SOL containing W back into the confined plasma.

There are significant differences in the average ELM W flushing efficiency for the three ELM types. The ELMs in the gas fuelled pulses are on-average, about half as efficient at flushing the W than the natural ELMs in the pellet fuelled pulses, while the pellet triggered ELMs are more efficient at flushing the W than the natural ELMs with either fuelling method. This is not simply a result of change to the density losses $\Delta \bar{n}_e / \bar{n}_e$, which show the opposite trend with ELM type. Although the pellets result in lower net density losses following the triggered ELM, more W is flushed from the plasma than after natural ELMs.

There are also significant differences in the inter-ELM W fluence data between the natural and pellet triggered ELMs. On average, considerably more W is able to enter the plasma

following the pellet triggered ELMs. Also, more W enters the plasma after either ELM type in pellet + gas fuelled pulses than gas-only fuelled pulses. Note that the average magnitudes of the ELM W flushing and inter-ELM ingress are similar, so the net change in the W content of the plasma is a delicate balance between these processes. In section 2.10 below, we investigate how differences between the pedestal and mantle gradient parameters might affect the transport of W in the edge plasma.

2.9. Influence of ELM type on sputtered impurity sources

Other than affecting the ELM W flushing efficiency and inter-ELM ingress of W into the plasma, the pellets might also affect the sources of impurities sputtered by the ELMs from the PFCs. In this section, we compare relative intra-ELM fluences, i.e. influxes integrated over the duration of the ELM peak in the line intensity signal, of Be and W impurities $\Phi_{Be, W}$ sputtered from the inner and outer divertor targets by the interaction with the ELMs.

A relative measure of these fluences can be estimated from time-integrated Be II (527 nm) and WI (401 nm) line intensities measured by a multi-chord spectrometer viewing the HFS, and LFS divertor targets. The lines of sight of this spectrometer are shown in figure 13(a). Profiles of the Be II (527 nm) and WI (401 nm) line intensities time-integrated over the ELM peak are shown in figure 13(b) as a function of the distance S along the divertor target. The most intense interaction with

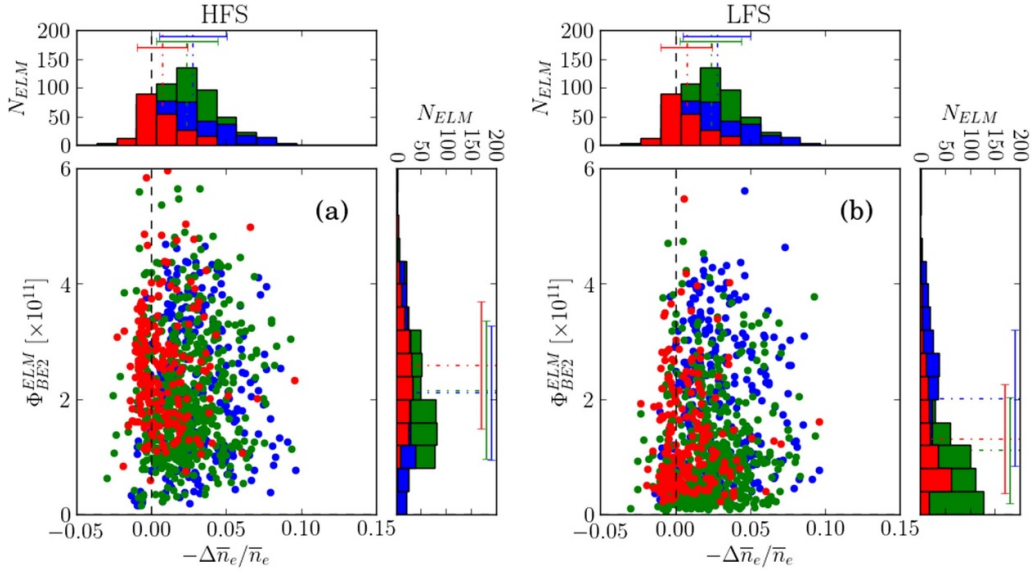


Figure 14. Comparison of data from the same high-power, 3.5 MA/3.3 T pulses as for figure 12 with only gas (●) and with pellet and gas fuelling (●, ●), for pellet-triggered (●) and natural (●, ●) ELMs, showing: relative, time-integrated, intra-ELM fluences of Be^+ ions Φ_{Be}^{ELM} measured by a multi-channel visible-range spectrometer (KS3) viewing the divertor region, spatially integrated over: (a) the HFS and (b) the LFS divertor targets. As in figure 12, the histograms show PDFs of the respective quantities for the different ELM types.

the ELM is with the top of the inner and outer vertical targets *aka* ‘domes’ and also at the strike points [51]. Also shown in figures 13(c) and (d) are the evolution of the Be II (527 nm) and WI (401 nm) line intensities, summed over channels viewing the inner and outer divertor targets, over the duration of a typical type-I ELM, indicating the period over which the intra-ELM fluences are integrated.

Note that the inner strike point is hidden from view in this corner-corner (C-C) configuration in which the both strike points are close to the divertor pumping throats, so these measurements are unable to detect the impurity influxes from the vicinity of outer strike point. It has been shown from the analysis of spectrally filtered, fast-camera imaging data from JET-ILW that the intra-ELM sputtered W^0 influx is almost an order of magnitude larger than the time-integrated inter-ELM influx from the strike-point regions [54].

In figures 14(a) and (b), relative, intra-ELM Be^+ fluences Φ_{Be}^{ELM} estimated (assuming constant ionisations/photon, S/XB) from the time-integrated Be II (527 nm) line intensity data summed over the HFS and LFS divertor targets respectively, plotted versus the relative ELM density losses $\Delta\bar{n}_e/\bar{n}_e$. Similar data for the relative W^0 atomic, intra-ELM fluences Φ_W^{ELM} are shown in figure 15. Average values of these fluences $\langle\Phi_{Be}\rangle$ and $\langle\Phi_W\rangle$ with their standard deviations are stated in table 6. The bremsstrahlung contribution to the WI line, detected by a LOS viewing through the x -point, which does not view a region of the target with significant interaction with the SOL plasma, is estimated to be $\lesssim 10\%$ during the intra-ELM periods.

The high degree of scatter in the relative ELM-sputtered Φ_{Be}^{ELM} and W^0 fluence data is shown in figures 14 and 15 is due to the similarly large spread in the ELM amplitudes. The averaged values over the whole data set, classified by fuelling source and ELM type, reveal little significant difference between these fluences at the HFS target between these cases,

except that the natural ELMs sputter slightly less W impurities ($\sim \times 0.8$) and the pellet-triggered ELMs slightly more Be ($\sim \times 1.15$) than the average over all ELMs. This is reversed at the LFS target, where the natural ELMs in the gas-only fuelled pulses do sputter significantly more W and Be ($\sim \times 1.2$ and 1.4 respectively) than the average over all ELMs.

Values of ionisations/photon (S/XB) for these Be and W lines available from the ADAS atomic database [48], increase with both T_e and n_e , as does the fraction of W^+ ions promptly redeposited at the surface [3]. Hence, without T_e and n_e data with sufficient temporal ($\mathcal{O}(100 \mu s)$) and spatial resolution ($\mathcal{O}(1 \text{ cm})$) measured at the divertor target surface, it is impossible to evaluate absolute influxes from the measured intensities. However, by assuming fixed values of S/XB and assuming that the measured Be^+ influx is equal to the incident flux at the targets, i.e. assuming a balance between erosion and redeposition, it is possible to calculate an effective sputtering yield for W by Be^+ ions $\gamma_{Be^+ \rightarrow W}$.

For intra-ELM conditions, typical S/XB values at $T_e = 100 \text{ eV}$ and $n_e = 10^{19} \text{ m}^{-3}$ of $(S/XB)_{WI} = 46.7$ and $(S/XB)_{BeII} = 52.5$ correspond to an S/XB ratio of 0.89 for the two lines, consistent with that used for a previous measurement on JET-ILW [55]. Resulting values for the intra-ELM sputtering yield lie in the range $\gamma_{Be^+ \rightarrow W} \sim 0.5\text{--}1.0$. These are consistent with values shown in figure 9 of [55], which were obtained using the same diagnostic, assumed S/XB values and spectrometer on JET-ILW.

In [55], it was shown that such high values for $\gamma_{Be^+ \rightarrow W} \sim 0.5\text{--}1.0$ are higher than that possible for Be^+ ions on W from physical sputtering, which has a maximum yield of $\gamma_{Be^+ \rightarrow W} \sim 0.4$. Hence, there must be a significant contribution from W sputtering by the incident D^+ fuel ions during type-I ELMs at the prevailing pedestal temperatures in JET-ILW. Also, conditional averaging of the resulting data reveals no significant

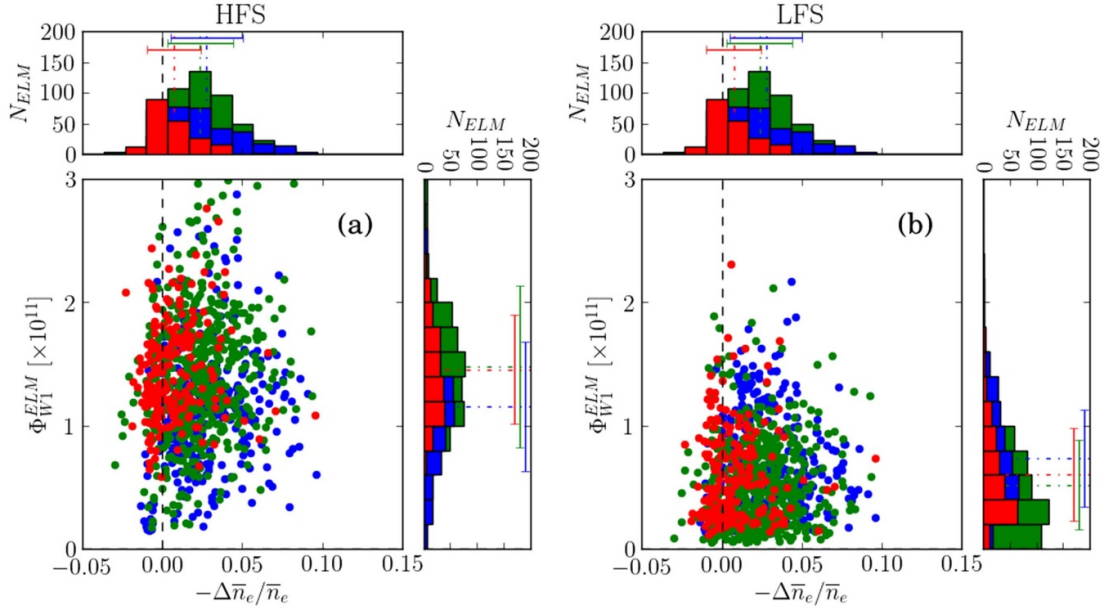


Figure 15. Comparison of data from the same high-power, 3.5 MA/3.3 T pulses as for figure 12 with only gas (●) and with pellet and gas fuelling (●, ●), for pellet-triggered (●) and natural (●, ●) ELMs, showing: relative, time-integrated, intra-ELM fluences of W^0 atoms Φ_{W1}^{ELM} measured by a multi-channel visible-range spectrometer (KS3) viewing the divertor region, spatially integrated over: (a) the inner (HFS) and (b) the outer (LFS) divertor targets. As in figure 12, the histograms show PDFs of the respective quantities for the different ELM types.

Table 6. Average values of the relative intra-ELM Be^+ and W^0 fluence data $\langle\Phi_{Be}\rangle$ and $\langle\Phi_W\rangle$, classified by fuelling source and ELM type for the data shown in figures 14 and 15 from high-power, 3.5 MA pulses. The sum of these fluences from both HFS and LFS targets is also stated.

Fuelling	ELM type	HFS		LFS		Total	
		$\langle\Phi_W\rangle$	$\langle\Phi_{Be}\rangle$	$\langle\Phi_W\rangle$	$\langle\Phi_{Be}\rangle$	$\langle\Phi_W\rangle$	$\langle\Phi_{Be}\rangle$
—	—	(a.u.)	(a.u.)	(a.u.)	(a.u.)	(a.u.)	(a.u.)
Gas-only	Natural	1.15 ± 0.03	2.11 ± 0.07	0.73 ± 0.02	2.02 ± 0.07	1.88 ± 0.05	4.13 ± 0.12
Pel and Gas	Pellet	1.48 ± 0.03	2.16 ± 0.05	0.52 ± 0.02	1.11 ± 0.04	2.00 ± 0.04	3.27 ± 0.10
—		1.46 ± 0.03	2.59 ± 0.08	0.60 ± 0.03	1.32 ± 0.07	2.06 ± 0.05	3.91 ± 0.13
—	All	1.38 ± 0.02	2.23 ± 0.04	0.60 ± 0.01	1.42 ± 0.03	1.97 ± 0.03	3.65 ± 0.07

difference in the measured sputtering yield $\gamma_{Be^{4+} \rightarrow W}$ by the different classes of ELMs.

2.10. Effect of pellets on pedestal and mantle parameters

We have seen above in section 2.4 that the amount of W in the plasma is a result of a delicate balance between the influx across the pedestal driven by inward neo-classical convection and the flushing of the W by the ELMs. Also, the in the high-power ITER-baseline pulses investigated here, the W is typically localised by outward neo-classical convection to the outer, mantle region, hence mitigating the tendency for this to accumulate in the plasma core.

In this section, we quantify the effect of the ELM pacing pellets on the density and temperature gradients in the pedestal and mantle regions during the inter-ELM periods following the pellet triggered ELMs, comparing the derived quantities ζ_{NC} and $\eta_e = L_{n_e}/L_{T_e}$ (which govern

the neo-classical impurity convection and provide the drive for electron-temperature-gradient (ETG) driven turbulence, respectively) during inter-ELM periods following the pellet-triggered or natural, spontaneous ELMs.

Pedestal characteristics $T_{e,ped}$, $n_{e,ped}$ and $p_{e,ped}$ and gradient parameters derived from $mtanh()$ fits to n_e and T_e profile data from the high-resolution, Thomson scattering system (HRTS) [29] are shown in figure 16. Values of the gradient parameters R/L_{T_e} , R/L_{n_e} and R/L_{p_e} and the derived parameters ζ_{NC} and η_e are spatially averaged over the pedestal $\langle \dots \rangle_{ped}$ and mantle $\langle \dots \rangle_{man}$ regions. In this figure the colour represents the type of the ELM preceding the HRTS measurement, i.e. whether the ELMs are pellet-triggered or natural ELMs in either gas-only or pellet + gas fuelled pulses.

In order to determine whether the ELM-pacing pellets have any statistically significant effect on the average values of the parameters ζ_{NC} and η_e over the pedestal and mantle regions, the data shown in figure 16 is plotted in figure 17 in the form

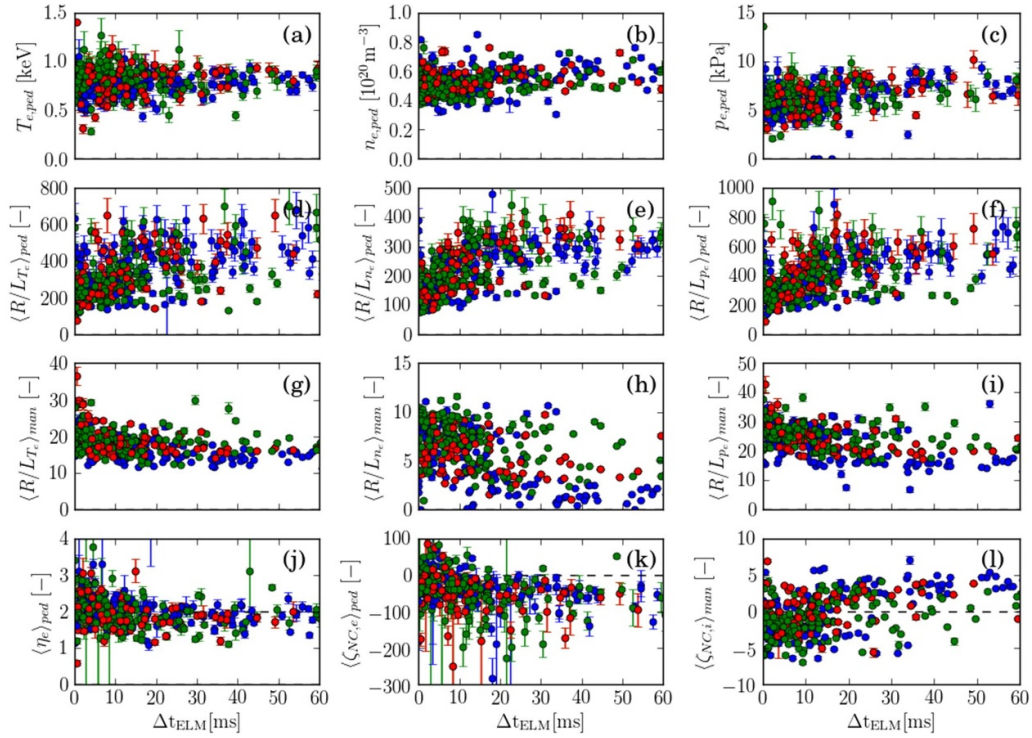


Figure 16. Inter-ELM evolution of parameters determined from fits to HRTS n_e and T_e profile data as a function of the time from the previous ELM Δt_{ELM} for the same six 3.5 MA/3.3 T ITER-baseline pulses as analysed in section 2.8, showing: the pedestal top parameters $T_{e,ped}$, $n_{e,ped}$ and $p_{e,ped}$ (a)–(c); their normalised gradients R/L_{T_e} , R/L_{n_e} and R/L_{p_e} averaged over the pedestal $\langle \dots \rangle_{ped}$ (d)–(f) and mantle regions $\langle \dots \rangle_{man}$ (g)–(i); and the parameter $\langle \eta_e \rangle_{ped}$ averaged over the pedestal region (j) and the neo-classical convection parameter averaged over the pedestal $\langle \zeta_{NC} \rangle_{ped}$ (k) and mantle regions $\langle \zeta_{NC} \rangle_{man}$ (l). The colours indicate the previous ELM type: natural ELMs in the gas fuelled pulses (●); natural ELMs (●) or pellet triggered ELMs (●) in pulses with pellet + gas fuelling.

of histograms, where the data is distinguished according to the preceding ELM type. Average values and standard deviations of the data (σ_{data}), also shown in figure 17, are stated in table 7.

Referring to the values of $\langle \zeta_{NC} \rangle_{ped}$ in table 7, we see that on-average there is relatively strong inward impurity convection ($\langle \zeta_{NC} \rangle_{ped} \sim -(30-50)$) across the pedestal during the inter-ELM periods. However, the time-resolved data shown in figure 16 shows that, during the first ~ 10 ms after the pellet-triggered and natural ELMs in the pellet fuelled pulses (●, ●), there is some tendency for this convection to weaken (and sometimes even reverse) due to the relatively lower $\langle R/L_{n_e} \rangle_{ped}$ following these ELMs. There is hence some tendency for the pacing pellets to reduce the inward W influx just after the ELMs.

In the mantle region, the overall average value of $\langle \zeta_{NC} \rangle_{man} \sim 0.14$ following all of the ELMs is much weaker than that prevailing in the pedestal region ($\langle \zeta_{NC} \rangle_{ped} \sim -(30-50)$). On-average, there is a somewhat higher, positive value of $\langle \zeta_{NC} \rangle_{man} \sim 0.24$ following the pellet triggered ELMs due to the fuelling at the pedestal top by the pellets reducing $\langle R/L_{n_e} \rangle_{man}$. However, after the natural ELMs in the pellet fuelled pulses, there is a slightly negative average value of $\langle \zeta_{NC} \rangle_{man} \sim -1.1$, driving inward impurity convection. This probably arises because of relatively low level of gas fuelling in the pellet fuelled pulses results in a slightly lower $n_{e,ped}$ than in the gas fuelled pulses and hence a higher value of $\langle R/L_{n_e} \rangle_{man}$, which favours inward impurity convection.

Hence, while the ELM pacing pellets do modify the pedestal gradients on-average such as to slightly increase the convection of W (and other impurities) across the pedestal, they also modify the mantle gradients to reduce the screening of these impurities from the plasma core.

Somewhat as an aside to the topic of this paper, the average values of η_e in the pedestal and mantle regions are worthy of note. As was discussed in [8] with respect to the high-power, 3 MA ITER-baseline pulse #92 432, the value of η_e averaged over the steep density gradient region ($\rho_{N,ped} \leq \rho_{tor} \leq 1.0$) of $\langle \eta_e \rangle_{ped} \sim 2$ as stated in table 7 for the 3.5 MA pulses are similar to those that were found for pulse #92 432, which may indicate that there may be a degree of stiffness of the electron heat transport in the pedestal, predominantly due to the slab branch of ETG turbulence, which is destabilised at a critical $\eta_e \sim \mathcal{O}(1)$. Note that, on-average, there is also an increase in $\langle \eta_e \rangle_{ped}$ during the first ~ 10 ms following the ELMs, providing a stronger drive for turbulent electron heat transport at this time.

Turning our attention now to the mantle region ($0.7 \leq \rho_{tor} \leq \rho_{N,ped}$), the average value of $\langle \eta_e \rangle_{man} \sim 3-5$ is larger than in the pedestal region, which may be consistent with the higher values of η_e required to destabilise the toroidal branch of ETG turbulence at the relatively low values of $\langle R/L_{n_e} \rangle_{man} \sim 5-10$ prevailing in the mantle compared to those in the pedestal region ($\langle R/L_{n_e} \rangle_{ped} \sim \mathcal{O}(-100)$). For further discussion of this topic see section 4 of [8].

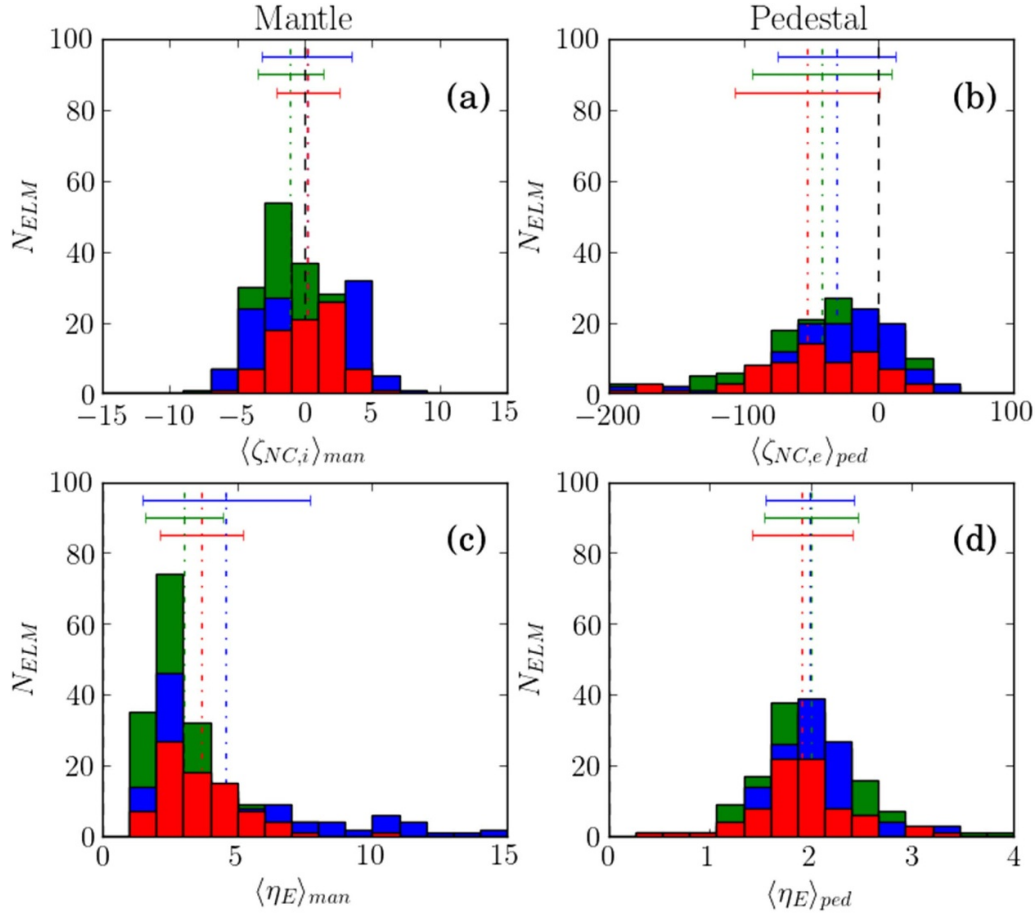


Figure 17. PDFs of the gradient parameters: ((a), (b)—top) ζ_{NC} and ((c), (d)—bottom) η_e shown in figure 16 for 3.5 MA ITER-baseline pulses, spatially-averaged over the mantle ((a), (c)—left) and density pedestal ((b), (d)—right) regions, where the data points have been selected by the ELM type preceding the HRTS measurement times: natural ELMs in the gas fuelled pulses (●) and natural ELMs (●) or pellet triggered ELMs (●) in pulses with pellet + gas fuelling.

Table 7. Average values of data shown in figure 17 by fuelling source and ELM type for high-power, 3.5 MA ITER-baseline pulses.

Fuelling	ELM type	ζ_{NC}		η_e	
		Pedestal	Mantle	Pedestal	Mantle
Gas-only	Natural	-30 ± 4	0.16 ± 0.2	2.0 ± 0.4	4.5 ± 0.3
Pel and Gas	Pellet	-42 ± 4	-1.1 ± 0.2	2.0 ± 0.4	3.1 ± 0.1
—	All	-52 ± 6	0.24 ± 0.3	1.9 ± 0.6	3.7 ± 0.2
—	All	-40 ± 2	0.14 ± 0.2	2.0 ± 0.3	3.7 ± 0.2

3. Discussion

3.1. Proposed mechanism for the influence of W radiation on the evolution of high-power, ITER-baseline pulses in JET-ILW

As mentioned in the introduction, sustained H-mode operation of JET-ILW pulses requires fuelling by gas puffing to mitigate the detrimental effect of W impurities sputtered from the divertor targets, predominantly but not exclusively by the extremely high instantaneous powers deposited by the ELMs. The beneficial effect of the gas puffing on this process is illustrated systematically in figure 18.

Although the physics underlying each step is not always well understood, the underlying mechanism can be explained as follows:

(a) Effect of increased gas fuelling on ELMs:

More gas fuelling typically increases the ELM frequency f_{ELM} and reduces the ELM energy losses ΔW_{ELM} (at approximately constant $\langle P_{ELM} \rangle$), resulting in a lower sputtered W source S_W from the divertor targets. A lower W concentration c_W in the SOL then reduces the impurity influx to the confined plasma between ELMs Φ_W^m and

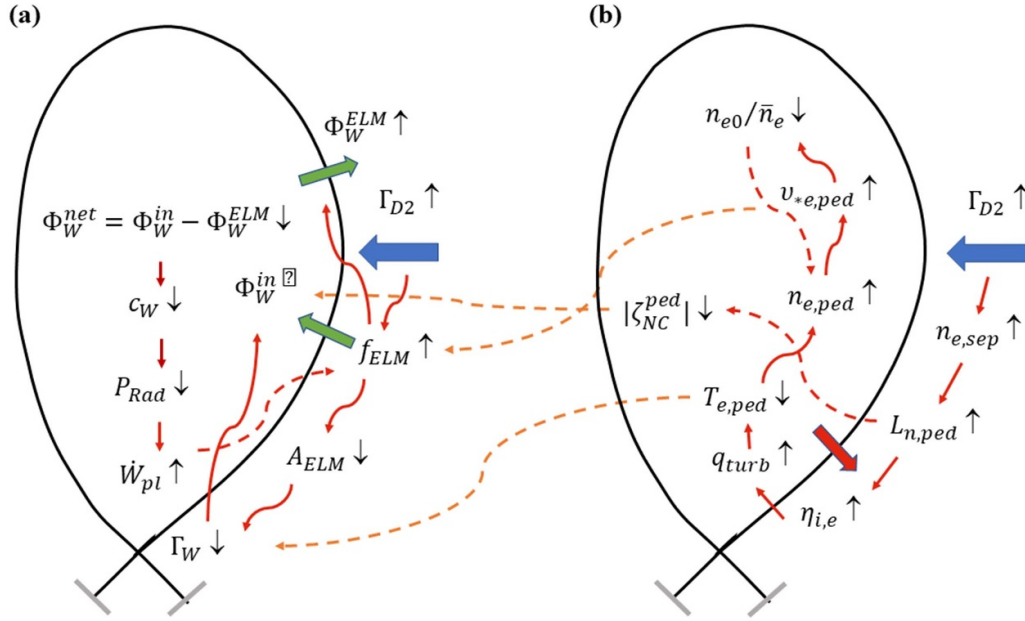


Figure 18. Schematic representation of the effect of gas puffing on: (a) the ELM behaviour and W radiation and (b) the inter-ELM pedestal characteristics.

the higher ELM frequency flushes more W out again Φ_W^{ELM} . A lower W concentration in the confined plasma then reduces the radiated power P_{Rad}^{Pl} , thereby increasing the rate of increase of stored energy dW_{pl}/dt between the ELMs. This causes $p_{e,sep}$ to reach the MHD pressure limit faster, triggering the ELMs earlier and thereby increasing their frequency f_{ELM} . The chain of causality of the effects of increased gas fuelling are illustrated in figure 18(a).

(b) *Effect of increased gas fuelling on pedestal and confinement:*

Although the effect of the gas fuelling on the inter-ELM pedestal structure is beneficial in terms of further mitigating the W contamination, it also reduces the energy confinement by degrading the pedestal temperature, which reduces the temperature over the whole plasma due to stiffness of core heat transport. An increase in turbulent heat flux across the pedestal due to changes in its structure caused by the gas puffing is now well established as the most plausible explanation for the low pedestal temperature in JET-ILW pulses [10, 12, 14, 56, 57] and this is illustrated schematically in figure 18(b).

Increased gas puffing raises the separatrix density $n_{e,sep}$, which decreases the density gradient across the pedestal, increasing L_{ne} and hence $\eta_{i,e}$ across the ETB, providing a stronger drive for turbulent heat transport. With the residual power through the ETB P_{Sep}^{iELM} determined by the heating power, radiation and ELM losses, an increase in the heat turbulent heat diffusivity χ_{eff} must reduce the pedestal temperature $T_{e,ped}$.

As a consequence of reducing $T_{e,ped}$, a higher pedestal density $n_{e,ped}$ is required for $p_{e,ped}$ to reach the peeling-ballooning limit at which ELMs are triggered. The lower $T_{e,ped}$ and higher $n_{e,ped}$ increases the effective collisionality $\nu_{eff} \propto n_e/T_e^2$ at the pedestal top. This

then reduces the density peaking $n_{e,0}/\bar{n}_e$, which is partly driven by a turbulent particle pinch, thereby reinforcing the higher $n_{e,ped}$ [58].

Conversely, less gas fuelling is required with the pellets, resulting in reduced $n_{e,ped}$ and higher $T_{e,ped}$ and lower ν_{eff} , which favours density peaking. This is then further reinforced by the more peaked beam ionisation source resulting from the reduced $n_{e,ped}$, which is known to play an important role in peaking the density profile in JET-ILW [59].

(c) *Feedback loops between gas puffing, ELMs and W behaviour:*

As indicated in figure 18, there is coupling between the changes to the pedestal structure, the ELM behaviour and the W transport, which reinforce the effects of the gas puffing. Firstly, the higher L_{ne} reduces the magnitude of the inward convection ζ_{NC} across the ETB, which reduces the W influx Φ_W^{in} into the confined plasma. Secondly, the lower $T_{e,ped}$ and higher $n_{e,ped}$ reduces T_e at the W targets during the ELM crashes, decreasing the incident ion energies and hence the physical sputtering yield and thereby reducing the W source. Also, more gas puffing typically increases f_{ELM} , flushing more impurities from the plasma¹⁸.

3.2. Understanding the evolution of pulse #92 432

We can try to use this insight into the effect of gas puffing on the pedestal and the W flushing by the ELMs to understand

¹⁸ Stability analysis reveals that at high puffing rates, when the pedestal collisionality $\nu_{*,e}$ is higher, the ELMs are triggered at well below the peeling-ballooning boundary and have more the character of resistive, type-III than type-I ELMs [10].

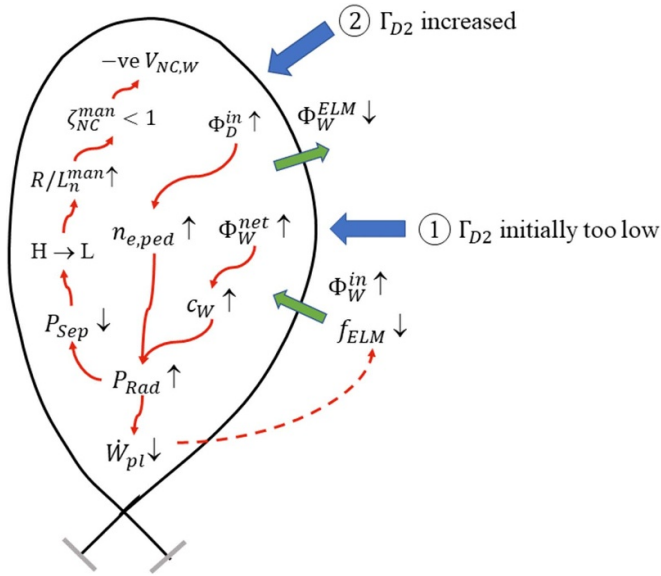


Figure 19. Schematic representation of the factors affecting the evolution of the high-power baseline scenario JET-ILW pulse #92 432 at: (1) the initial phase and (2) after the feedback system increases the gas puffing rate Γ_{D2} to try to control the W influx.

the evolution of the high-power, 3 MA baseline-scenario pulse #92 432, which was discussed in detail in section 2.6. A schematic representation of the causality of the underlying mechanisms is shown in figure 19. A breakdown of this mechanism follows:

- Initially, the rate of gas fuelling was probably too low, causing a gradual buildup of the W content, increasing P_{Rad}^{Pl} , decreasing dW_{pl}/dt and hence causing a reduction of the ELM frequency f_{ELM} (see figure 10).
- In response to the decrease in f_{ELM} , the plasma control system initiated an increase in the gas puffing rate Γ_{D2} , which had the opposite effect to that desired. More gas fuelling raised $n_{e,ped}$, consequently increasing P_{Rad}^{Pl} , reducing dW_{pl}/dt and hence further reducing f_{ELM} , eventually stopping the ELMs entirely.
- Cessation of the ELMs caused $n_{e,ped}$ to rise faster, resulting in an even faster increase in mantle radiation $P_{Rad}^{man} \propto \langle C_W n_e^2 \rangle_{Man}$, hence strongly reducing $P_{Sep}^{iELM} = P_{l,th} - P_{Rad}^{Pl}$.
- Once P_{Sep}^{iELM} falls sufficiently, this triggers an H/L-transition, which rapidly reduces $n_{e,ped}$ and increases R/L_{ne} in the mantle region.
- The increased $\langle R/L_{ne} \rangle_{man}$ then causes sudden reversal of the neo-classical convection ($\langle \zeta_{NC} \rangle_{man} < 0$), driving the W impurities into the plasma core, causing a reduction in $T_{e,0}$, a collapse in W_{pl} , ending the high-performance phase of the pulse.

Note that this particular pulse does in fact recover from the W accumulation event. The L-mode phase is followed by another period of ELMy H-mode, albeit with higher P_{Rad} and reduced energy confinement.

3.3. W impurity retention and redeposition in the divertor

The fraction of radiated power \mathcal{F}_{Rad} is higher in the pellet + gas-fuelled pulse #96 713 compared to that in the gas-fuelled pulse #94 980, in spite of the fact that on-average, the level of inter-ELM Be influx $\langle \Gamma_{Be} \rangle$ from the target is comparatively lower (see figures 1(f) and (g)). Although the level of ELM-sputtered W from the targets is lower in pulse #96 713, the W concentration in the mantle $\langle C_W \rangle_{man}$ is higher than in pulse #94 980 (see figure 11(a)). This implies that the retention [60, 61] and/or prompt re-deposition [3] of the sputtered W in the divertor is less efficient in pulse #96 713, which has a lower ($\sim 45\%$) gas fuelling rate than that in pulse #94 980.

The process of prompt redeposition of the sputtered W^0 is due to singly ionized W^+ ions being redeposited with their first Larmor orbit onto the target. This occurs because the Larmor radius ρ_{W^+} of the heavy ($m_W/m_p \sim 183$) W^+ ions can be larger than the ionization length L_0^{19} of the sputtered W^0 atoms [3]. The fraction of ions redeposited to the target f_{dep} decreases with an increase of the ratio of ionisation length to the W^+ Larmor radius $p = L_0/\rho_{W^+}$ according to $f_{dep} \propto 1/(1+p^2)$ [62]. This ratio p decreases with increasing density $n_{e,t}$ and electron temperature $T_{e,t}$ at the target. It is hence difficult to predict the effect of increasing the gas puffing on f_{dep} without complex modelling, e.g. with the kinetic impurity simulation code ERO [63], and knowledge of how $n_{e,t}$ and $T_{e,t}$ respond to the changes in fuelling.

The relatively higher $\sim \times 1.5$ concentration of W in the pellet + gas fuelled pulse #96 713 compared to that in the gas fuelled pulse #94 980 might also be a sign of reduced retention of the sputtered W in the divertor. Modelling the transport of W ($Z_W = 74$), which has many ionisation states, in the SOL plasma is computationally extremely complex. Some insight into the processes involved can be gleaned from inspection of the parallel force balance on the impurity ions, which is stated as equation (1) of [60]. The relevant terms (where I represents impurity ions) are: (1) $m_i n_i n_I \langle \sigma_i v \rangle (U_{\parallel,i} - U_{\parallel,I})$ representing friction with other ion species; and (2) $\alpha_{I,i} Z_I^2 n_I \nabla_{\parallel} T_I$ and $\alpha_{I,e} Z_I^2 n_I \nabla_{\parallel} T_e$ representing thermal forces due to the parallel temperature gradients of the ions and electrons. Here, $U_{\parallel,i/I}$ are the average parallel flow speeds of the respective ions i/I , $\langle \sigma_i v \rangle$ is the momentum exchange rate between ions and impurities and the $\alpha_{I,i/e}$ are coefficients for the ion/electron thermal forces.

It might be expected that, with an increased gas fuelling rate $\Gamma_{D2,gas}$ into the main chamber, that with the increased flow of D^+ ions through the SOL to the divertor, the parallel friction force (1) might increase, thereby enhancing the retention of the W impurities in the divertor. A higher parallel temperature gradient in the SOL would, however, act to reduce the impurity retention by increasing the thermal forces (2), which are directed away from the target. Without detailed modelling with a SOL transport code, it is not easy to determine how $\nabla_{\parallel} T_e$ will change along the SOL in response to changes in the fuelling and how these changes will influence the impurity retention.

¹⁹ The ionisation length is defined as $L_0 = v_0 / (S_0 n_e)$, where S_0 is the ionisation rate coefficient of the W_0 atoms and v_0 is their speed.

In conclusion, it may well be that increased W retention and also an increase in the prompt redeposition fraction with a higher $n_{e,t}$ at higher fuelling rate might explain the lower W concentration in pulse #94980 cf that in pulse #96713. Exhaustive modelling, e.g. with a SOL transport code such as SOLPS [64] or the latest ITER version SOLPS-ITER [65], is required to elucidate these effects further.

Finally, it is worth noting that, if there is a balance between the incident Be flux to the target and that sputtered during the inter-ELM periods, the comparatively lower intra-ELM Be influx in pulse #96713 implies, a lower rate of Be sputtering by the ELMs from the main chamber walls, which are faced with Be tiles. The ELM-sputtered Be influx from the walls might be expected to decrease with a lower neutral gas density in the plasma-wall interspace, resulting from reduced gas puffing into the main chamber in pulses with pellet + gas fuelling.

4. Conclusions

ITER-baseline scenario pulses typically operate at a higher plasma current I_p and consequently, lower $\beta_N = \beta_T(B_t/aI_p) \sim 1.8$ – 2^{20} and lower edge safety factor $q_{95} \sim 3$, e.g. than hybrid-scenario pulses, which operate at lower I_p and hence higher $\beta_N \sim 2$ – 3 and $q_{95} \sim 4$. Because the pedestal density $n_{e,ped}$ increases with I_p [11], the higher $I_p \leq 4$ MA of baseline-scenario pulses results in a relatively higher $n_{e,ped}$ and less peaked n_e profile ($n_{e,0}/\bar{n}_e \sim 1.3$) than in hybrid-scenario pulses with $n_{e,0}/\bar{n}_e \sim 2.2$.

The high $n_{e,ped}$ and low n_e peaking in baseline-scenario pulses has a fortuitous effect on the impurity transport and hence the radiation, which favours steady-state ELMy H-mode operation. The weak n_e gradient and hence low normalised gradient R/L_{n_i} across the core plasma compared to that of T_i , typically results in outward neo-classical impurity convection $\zeta_{NC} = R/2LT_i - R/L_{n_i} > 0$ and hence a hollow impurity density profile. This localises the strongly radiating W impurities to the mantle region, where they can be efficiently flushed from the confined plasma by the ELMs.

This strong W radiation from the mantle has a dominant effect on the electron power balance there and, without efficient flushing by the ELMs, this can reduce the power crossing the separatrix P_{Sep} , hence slowing and even stopping the ELMs altogether, which often causes a runaway radiation event, an H/L-transition and sudden impurity accumulation. This is one of the main causes of the higher disruptivity of high-power, H-mode pulses in JET-ILW [5].

Note that, because hybrid-scenario pulses are run at lower I_p and higher β_N , these operate with a lower $n_{e,ped}$ and hence more peaked n_e profile. Consequently, such pulses are more prone to core W accumulation and can often suffer from radiation collapse of the central electron temperature, leading to a disruption. In such pulses, which are characterised by a broad,

elevated q profile with $q_0 \gtrsim 1.0$, the W accumulation is usually triggered by low- n NTMs, which are destabilised at low-order rational surfaces, e.g. $m/n = 3/2, 4/3, \dots$. The physics of this process has been investigated in detail in [16].

As mentioned earlier, it has recently been demonstrated that optimised gas fuelling during the initial current ramp phase, can result in a hot, low collisionality pedestal, which effectively screens out the high- Z impurities from the confined plasma [17]. Similar analysis of the ELM flushing in such optimised, high-performance hybrid-scenario pulses has shown that the behaviour of the W impurities is quite different to that observed in baseline pulses, i.e. the ELMs do not flush but instead allow W to enter the confined plasma, which is then removed during the inter-ELM periods by outward neo-classical convection [66].

This ‘vicious circle’, i.e. the strong mantle radiation slowing and thereby stopping the ELMs flushing out the W impurities, in baseline-scenario pulses as illustrated by the radiation ‘event’ in pulse #92432 (see section 2.6), can be avoided by maintaining regular ELMs by the injection of small ELM-pacing pellets. The primary, beneficial effect of the ELM-pacing pellets, at a frequency $f_{Pel} \sim 25$ – 45 Hz into such pulses, is to maintain a regular ELM frequency $f_{ELM} \gtrsim f_{Pel}$, preventing the occurrence of ELM-free H^* -phases longer in duration than $\tau_{Pel} = 1/f_{Pel} \sim 20$ – 40 ms, which can lead to an H/L-transition and subsequent W accumulation or sometimes a disruption due to the strong radiation from the mantle.

A secondary, beneficial effect is that the use of the pacing pellets, which also fuel the plasma, allows operation with a reduced D_2 puffing rate into the main chamber, e.g. in pulse #96713 the 45 Hz pellets provide $\sim 60\%$ of the total D_2 fuelling rate. It is well established that an increased rate of gas fuelling is detrimental to the pedestal confinement and hence to the overall energy confinement, so the use of the pacing pellets allows the duration of the ELMy H-mode phase to be extended, while also maintaining good overall energy confinement.

The capability to run high-power plasmas with $P_{in} \lesssim 40$ MW, yielding a D-D neutron rate of $\Gamma_{n,DD} \gtrsim 5 \times 10^{16} \text{ ns}^{-1}$ (equivalent to a D-T fusion power $P_{DT} \sim 15$ MW) sustained for 5 s is one of the KPI for the JET-ILW C38 campaign, which is preparing for the forthcoming D-T campaign (DTE2). The evolution of the best performing, unseeded ITER-baseline scenario pulse #96482 achieved so far with pellets + gas fuelling is shown in figure 20. This pulse achieved a maximum D-D neutron rate of $\Gamma_{n,DD} \sim 4.15 \times 10^{16} \text{ ns}^{-1}$, with an average over the 5 s period 8–13 s of $\langle \Gamma_{n,DD} \rangle \sim 2.6 \times 10^{16} \text{ ns}^{-121}$.

It should be noted that record performance for an ITER-baseline scenario pulse in JET-ILW has been achieved so far using Ne impurity seeding in the 3 MA/2.8 T pulse #96994 with 31 MW heating power [17]. With a Ne seeding rate of $\Gamma_{Ne} \sim 0.5 \times 10^{22} \text{ e s}^{-1}$ and 45 Hz D_2 ELM pacing pellets, this pulse achieved a confinement enhancement factor $H_{98,y2} \sim 1.1$

²⁰ The normalised plasma pressure (toroidal beta) is defined as $\beta_T = \langle p_{pl} \rangle / (B_{t,0}^2 / 2\mu_0)$, where $\langle p_{pl} \rangle$ is the volume-averaged total plasma pressure.

²¹ Over the 3 s period of pulse #96482, 10–13 s, $\Gamma_{n,DD} \sim 3.1 \times 10^{16} \text{ ns}^{-1}$.

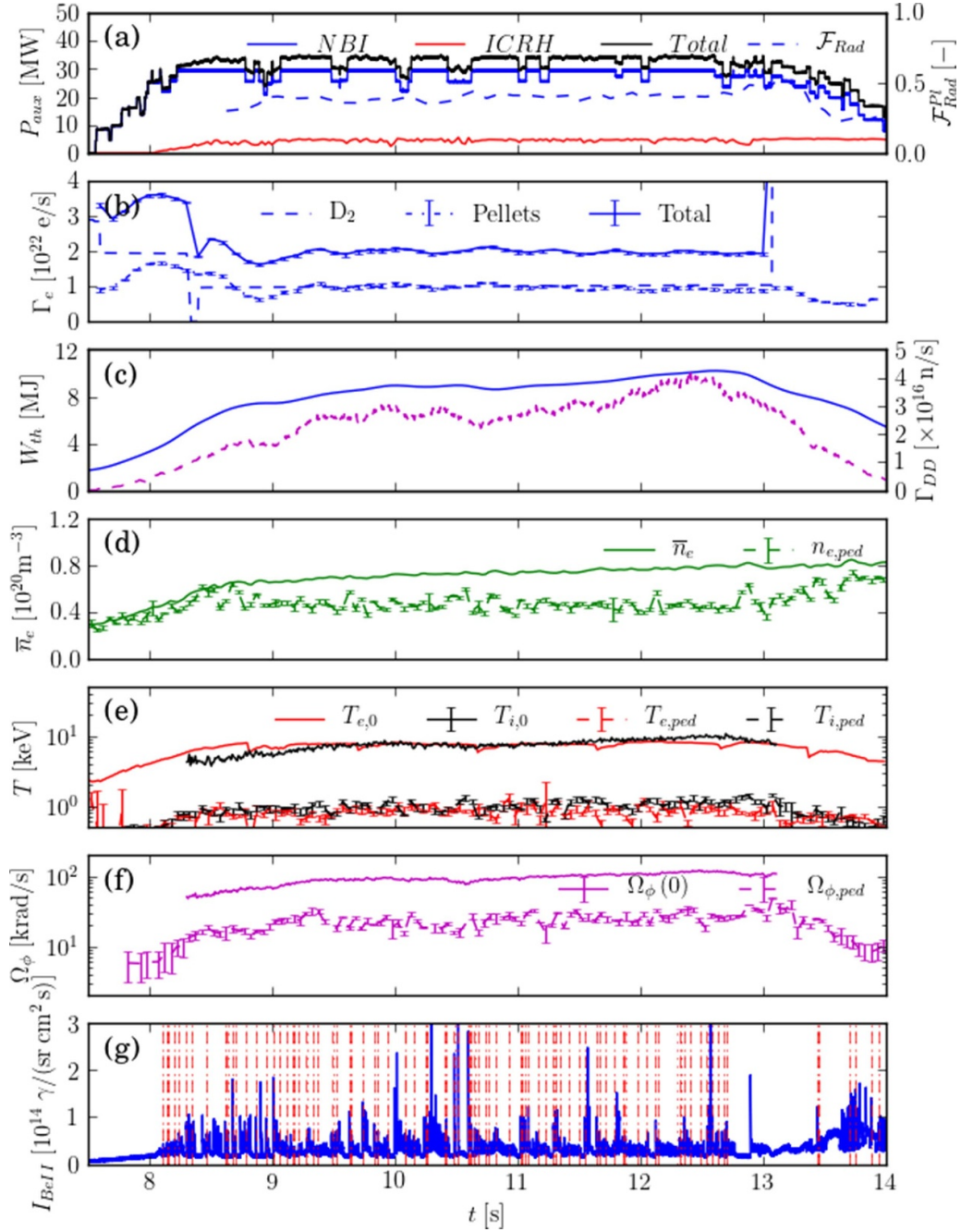


Figure 20. Evolution of high-performance 3.5 MA/3.3 T ITER-baseline scenario pulse #96482 with the record averaged ‘flat-top’ D-D neutron rate for an unseeded pulse, showing: (a) total absorbed additional heating power P_{abs} (solid) and radiated power fraction $\mathcal{F}_{Rad} = P_{Rad}/P_{abs}$ (dashed); (b) D₂ gas fuelling rate $\Gamma_{D2,gas}$ (dashed), smoothed pellet fuelling rate $\Gamma_{D2,pel}$ (dot-dashed) and total fuelling rate $\Gamma_{D2} = \Gamma_{D2,gas} + \Gamma_{D2,pel}$ (solid); (c) total MHD stored energy W_{th} (solid) and H-mode confinement enhancement factor $H_{98,y2}$ (dashed); (d) mid-plane, line-averaged density \bar{n}_e (solid) and D-D neutron rate $\Gamma_{n,DD}$ (e/s) (dashed); (e) axial electron and ion temperatures $T_{e,0}$ and $T_{i,0}$ (solid) and pedestal temperatures $T_{e,ped}$ and $T_{i,ped}$ (dashed), (f) axial $\Omega_{\phi,0}$ and pedestal $\Omega_{\phi,ped}$ toroidal rotation rates, (g) the ELM behaviour from a visible Be II line viewing the outer divertor target.

and a D-D neutron yield of $\langle \Gamma_{n,DD} \rangle \sim 3.1 \times 10^{16} \text{ ns}^{-1}$ averaged over 5 s.

In such high-power, pellet + gas fuelled, ITER-baseline pulses, the improved energy confinement is mainly caused by a increase in the ion energy confinement in the plasma core, relative to that of the electrons, rather than increased pedestal energy confinement [23]. This has several causes: (1)

decreased $n_{e,ped}$ and hence increased n_e peaking, results in more central NBI power and torque deposition; (2) increased toroidal rotation rate Ω_{ϕ} , and hence increased $E \times B$ flow shear across the core gradient region; (3) a higher T_i/T_e ratio across the core plasma, which results in an increased fraction of beam heating of the ions and is also stabilising to ITG turbulence and hence reinforces turbulence suppression by the $E \times B$ flow

shear. As well as these effects, in high-power JET-ILW pulses, the fast particle pressure p_{fp} can also play a role in stabilisation of ITG turbulence [67, 68].

A ‘virtuous circle’ due to synergy between the increase in core confinement and pedestal stability was suggested in [69]. The proposed mechanism is that a larger Shafranov shift due to higher β_N favours pedestal stability [64], thereby allowing a higher $p_{e,ped}$, which can then lead to an improvement of core confinement if the core heat transport is ‘stiff’. Note, however, that the time-averaged pedestal energy $\langle W_{th,ped} \rangle$ is not significantly higher in the pellet + gas fuelled pulse #96 713 compared to that in the gas fuelled pulse #94 980 investigated here. Also, the improved core confinement in #96 713 is likely due instead to decreased stiffness [70] of ion heat transport due to the relatively higher rotational $E \times B$ shear in pulse #96 713.

There are other, more subtle and mainly beneficial effects of the ELM-pacing pellets. The change in ELM characteristics to typically smaller amplitude, compound ELMs reduces time-averaged ELM-sputtered impurity influxes. There is also a temporary effect of the pellets on the pedestal gradients, decreasing the impurity convection across the pedestal and increasing their localisation to the mantle. However, the effect of the subsequent small, rapid ELMs on the mantle gradients is to reduce the efficacy of neo-classical impurity screening from the core.

Further pulses are to be run during the C38 campaign on JET-ILW at higher plasma current $I_p \lesssim 3.6 - 4.0$ MA, so it will be of interest to determine whether this increase results in an overall improvement in energy confinement. Whereas the $ITER - H98P(y, 2)$ scaling predicts increased energy confinement ($\tau_{E,th} \propto I_p^{0.9}$), this may be offset by a broader NBI power deposition profile with the increased pedestal density expected at high plasma current [11]. Higher $n_{e,ped}$ will increase the outward neo-classical convection of the W impurities, hollowing their density profile, and hence promote their flushing from the confined plasma by ELMs. However, the fact that the L/H-threshold power P_{LH} also increases with B_t [52] makes baseline scenario pulses more difficult to control at higher plasma current.

A risk with relying on pellet injection to control the W impurity content by promoting frequent ELMs is that any ‘missing’ pellets due to malfunction of the injector or pellets shattering in the flight tube would result in longer ELM-free phases, risking the occurrence of a radiation induced disruption. This places high demand on the reliability of the pellet injectors on ITER or a future fusion reactor.

It should be noted that high-performance H-mode operation is possible in JET-ILW without any gas or pellet fuelling during the ELMy H-mode phase. A new regime with small, high-frequency ELMs and neo-classical impurity screening due to the high core T_i gradient allows such pulses to run without severe W accumulation [71].

Data availability statement

The data that support the findings of this study will be openly available following an embargo at the following URL/DOI:

<https://git.ccf.ac.uk/afield>. Data will be available from 30 November 2021.

Acknowledgments

This work has been carried out within the framework of the EUROfusion Consortium and has received funding from the EURATOM Research and Training Programme 2014–18 and 2019–20 under Grant Agreement No. 633053 and from RCUK Energy Programme (Grant No. EP/T012250/1). To obtain further information on the data and models underlying this paper please contact PublicationsManager@ukaea.uk. The views and opinions expressed herein do not necessarily reflect those of the European Commission.

ORCID iDs

A R Field  <https://orcid.org/0000-0003-0671-9668>

L Garzotti  <https://orcid.org/0000-0002-3796-9814>

L Horvath  <https://orcid.org/0000-0002-5692-6772>

C M Roach  <https://orcid.org/0000-0001-5856-0287>

D van Eester  <https://orcid.org/0000-0002-4284-3992>

References

- [1] Garzotti L *et al* 2019 *Nucl. Fusion* **59** 076037
- [2] Hinnov E *et al* 1978 *Nucl. Fusion* **18** 1305
- [3] Naujoks D *et al* 1996 *Nucl. Fusion* **36** 671
- [4] Lux H *et al* 2014 ADAS Workshop 2014 (Cosner’s House, Abingdon, UK)
- [5] Pucella G *et al* 2021 *Nucl. Fusion* **61** 046020
- [6] Lerche E *et al* 2016 *Nucl. Fusion* **56** 036022
- [7] Giroud C *et al* 2013 *Nucl. Fusion* **53** 113025
- [8] Field A R *et al* 2020 *Plasma Phys. Control. Fusion* **62** 055010
- [9] Hatch D R *et al* 2019 *Nucl. Fusion* **59** 103135
- [10] Maggi C F *et al* 2015 *Nucl. Fusion* **55** 113031
- [11] Kallenbach A *et al* 2002 *Nucl. Fusion* **42** 1184
- [12] Hatch D R *et al* 2016 *Nucl. Fusion* **56** 104003
- [13] Hatch D R *et al* 2017 *Nucl. Fusion* **57** 036020
- [14] Kotchenreuther M *et al* 2017 *Nucl. Fusion* **57** 064001
- [15] Joffrin E *et al* 2019 *Nucl. Fusion* **59** 112021
- [16] Hender T C *et al* 2016 *Nucl. Fusion* **56** 066022
- [17] Garcia J *et al* 2020 Integrated scenario development at JET for DT operation and ITER risk mitigation 28th IAEA Fusion Energy Conference (FEC 2020) (10–15 May 2021) EX/1-2 Virtual
- [18] Geraud A *et al* 2012 Symposium on Fusion Technology 27th SOFT Conf. (Liège, Belgium, 24–28 September 2012) p 1.31
- [19] Lang P T *et al* 2013 *Nucl. Fusion* **53** 073010
- [20] Lawson J D 1955 *Proc. Phys. Soc.* **B70** 6–10
- [21] ITER Physics Expert Group on Confinement and Transport *et al* 1999 *Nucl. Fusion* **39** 2175
- [22] Field A R *et al* 2004 *Plasma Phys. Control. Fusion* **46** 981
- [23] Kim H T *et al* 2018 *Nucl. Fusion* **58** 036020
- [24] Hawryluk R 1979 An empirical approach to tokamak transport *Physics of Plasmas Close to Thermonuclear Conditions* (Varenna, Italy, 27 August–8 September 1979)
- [25] Lao L *et al* 1985 *Nucl. Fusion* **25** 1611
- [26] Appel L *et al* 2006 *Proc 33rd Conf. Contr. Fusion and Plasma Phys. (Rome, EPS Geneva)*
- [27] Ingesson L C *et al* 1998 *Nucl. Fusion* **38** 1675
- [28] Huber A *et al* 2007 *Proc. 24th Symp. Fusion Technology SOFT-24, Fusion Eng. and Design* vol 82 pp 1327–34

- [29] Pasqualotto R *et al* 2004 *Rev. Sci. Instrum.* **75** 3891–3
- [30] Andrew Y *et al* 2006 *Rev. Sci. Instrum.* **77** 10E913
- [31] Hawkes N C and Peacock N J *et al* 1992 *Rev. Sci. Instrum.* **63** 5164
- [32] Dickinson D *et al* 2011 *Plasma Phys. Control. Fusion* **53** 115010
- [33] Simpson J *et al* 2019 *Nucl. Mater. Energy* **20** 100599
- [34] Sertoli M *et al* 2018 *Rev. Sci. Instrum.* **89** 113501
- [35] Pankin A *et al* 2004 *Comput. Phys. Commun.* **159** 157–84
- [36] Brambilla M 1999 *Plasma Phys. Control. Fusion* **41** 1
- [37] Newton S and Helander P 2006 *Plasma Phys. Control. Fusion* **13** 012505
- [38] Lee J *et al* 2014 *Nucl. Fusion* **54** 022002
- [39] Goldston R 1985 Topics on confinement analysis of tokamaks with auxiliary heating basic processes of toroidal fusion plasmas (Proc. Course and Workshop, 1985) *Basic Proc. Toroidal Fusion Plasmas (Proc. Course and Workshop (Varenna, Italy))* 1986 Varenna, Italy EUR-10418-EU, Brussels, vol 1 p 165
- [40] Connor J W and Wilson H R 1994 *Plasma Phys. Control. Fusion* **36** 719
- [41] Hahm T T and Burrell K H 1995 *Phys. Plasmas* **2** 1648
- [42] Highcock E G 2012 *et al Phys. Rev. Lett.* **109** 265001
- [43] Houlberg W A *et al* 1985 *Phys. Plasmas* **4** 3230
- [44] Wesson J A *et al* 1997 *Nucl. Fusion* **37** 578
- [45] Angioni C *et al* 2015 *Phys. Plasmas* **22** 055902
- [46] Angioni C *et al* 2014 *Plasma Phys. Control. Fusion* **56** 124001
- [47] Fedorczak N *et al* 2015 *J. Nucl. Mater.* **463** 85–90
- [48] Summers H P *et al* 2006 *Plasma Phys. Control. Fusion* **48** 263
- [49] Henderson S S *et al* 2017 *Plasma Phys. Control. Fusion* **59** 055010
- [50] Carolan P G and Piotrowicz V A 1998 *Plasma Phys.* **25** 1065
- [51] Field A R *et al* 2017 *Plasma Phys. Control. Fusion* **59** 095003
- [52] Martin Y R *et al* 2008 *J. Phys.: Conf. Ser.* **123** 012033
- [53] Fundamenski W and Pitts R A 2007 *J. Nucl. Mater.* **363–365** 319
- [54] Huber A *et al* 2019 *Nucl. Mater. Energy* **18** 118–24
- [55] Den Harder N 2016 *Nucl. Fusion* **56** 026014
- [56] Maggi C F *et al* 2017 *Nucl. Fusion* **57** 11612
- [57] Hatch D P *et al* 2018 *Plasma Phys. Control. Fusion* **60** 084003
- [58] Weisen H *et al* 2005 *Nucl. Fusion* **45** L1
- [59] Garzotti L, Valović M and Garbet X *et al* 2006 *Nucl. Fusion* **46** 994
- [60] Senichenkov I U *et al* 2019 *Plasma Phys. Control. Fusion* **61** 045013
- [61] Stangeby P 2000 *The Plasma Boundary of Magnetic Fusion Devices* (Bristol & Philadelphia: IOP Publishing) (<https://doi.org/ISBN-750305592>)
- [62] Chankin A V *et al* 2014 *Plasma Phys. Control. Fusion* **56** 025003
- [63] Naujoks D *et al* 1994 *J. Nucl. Mater.* **210** 43
- [64] Schneider R *et al* 2006 *Contrib. Plasma Phys.* **46** 3–191
- [65] Wiesen S *et al* 2015 *J. Nucl. Mater.* **463** 480–4
- [66] Field A R *et al* 2021 Pedestal temperature gradient screening of high-Z impurities in optimised ‘hybrid’ scenario H-mode plasmas in JET-ILW (in preparation)
- [67] Citrin J *et al* 2013 *Phys. Rev. Lett.* **111** 155001
- [68] Citrin J *et al* 2015 *Plasma Phys. Control. Fusion* **57** 014032
- [69] Challis C *et al* 2015 *Nucl. Fusion* **55** 053031
- [70] Mantica P *et al* 2009 *Phys. Rev. Lett.* **102** 175002
- [71] Garcia J *et al* 2021 New plasma regimes with small ELMs and high confinement at the Joint European Torus *Phys. Rev. Lett.* (arXiv: [2103.02679](https://arxiv.org/abs/2103.02679))